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Prediction of Radar Pulse Envelope  
Distortion due to  
Tropospheric Propagation

Marina Ozerova

DSTO-TN-0125

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# Prediction of Radar Pulse Envelope Distortion due to Tropospheric Propagation

*Marina Ozerova*

**Electronic Warfare Division  
Electronics and Surveillance Research Laboratory**

DSTO-TN-0125

## **ABSTRACT**

This project is a part of research into the detection of radar signals at ranges well beyond the horizon by exploiting the effect of tropospheric scattering. A result of this work is a program written in C language which enables the distortion of the envelope of a given radar pulse, which occurs as a result of propagating over any path by tropospheric scattering, to be predicted.

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## EXECUTIVE SUMMARY

The objective of the work described in this report is to investigate the possibilities of detecting radar transmissions from very long range by means of tropospheric scattering.

The propagation of radio waves via the troposphere occurs as a result of a scattering mechanism which takes place in the volume of the tropospheric medium where the beams of the transmitting and receiving antennas overlap.

Radar signals which propagate via the troposphere will have a distorted pulse envelope shape due to the difference in the transit time between the shortest and longest paths from the transmitter to the receiver via the extremities of the scattering volume. The extent of the distortion will depend on the pulse duration compared to the time difference between propagation via the longest and shortest paths.

The main objective of the work described in this report was to predict the distortion of the pulse envelope shape of radar signals after propagation via the troposphere. In order to optimise the detection of tropospheric scattered radar signals it is desirable to be able to predict this distortion to enable a better matched filter to be designed.

The procedure adopted is to assume that the variations to the pulse shape result from the spatial distribution of the scattering and the scattering mechanism is equivalent to the reflection of the signal from a large number of point reflectors randomly distributed within the scattering volume.

## Author

### **Marina Ozerova** Wide Area Surveillance Division

*Marina Ozerova recently joined DSTO as a Professional Officer Class 1 in Wide Area Surveillance Division although the work described in this report was done in Electronic Warfare Division prior to her appointment. Marina was born in Russia and graduated from the Physics Faculty of Nizhny Novgorod State University in 1987. She defended her project on low temperature deposition of  $A_2B_6$  semiconductors using high frequency plasma thermo-decomposition of  $Cd(CH_3)_2$  and  $Te(CH_3)_2$  metal organic compounds widely used in infra-red detectors. Marina emigrated to Australia in 1993 and has since become an Australian Citizen. After arriving in Australia she undertook a number of work experience jobs to help adapt to the Australian work environment and to improve her command of English. Work experience included working as a Physicist for the Department of Mines and Energy, the Radiation Protection Branch of the S.A. Health Commission and, finally, with Electronic Warfare Division of the DSTO.*

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## 1. Introduction

The problem of scattering of electromagnetic waves in the troposphere attracts considerable attention from scientists and engineers. The phenomenon related to long-range atmospheric propagation of short waves beyond the limits of the "radio horizon" is known to be one of the least developed subjects of this kind.

Thus, the propagation of radio waves via the troposphere occurs as a result of the poorly understood mechanism of scattering which takes place in the volume of space where the beams of the transmitting and receiving antennas overlap.

The goal of this project was not to dwell on all the numerous problems associated with the use of radio scattering for the purpose of long range communication. Instead, the main objective of the current project were to predict the distortion of the pulse envelope shape of radar signals after propagation via the troposphere. The ability to predict the pulse envelope will enable a better matched filter to be designed for detecting the signals.

Radar signals which propagate via the troposphere will have a distorted pulse envelope shape if the difference in the transit time between the shortest and longest paths from the transmitter to the receiver, via the extremities of the scattering volume, is comparable with the pulse duration and in most instances this will be the case. In order to optimise the detection of tropospheric scattered radar signals it is desirable to be able to predict the pulse envelope distortion that will occur.

The area of our interest is in estimating the variations to the pulse shape and since this envelope shape distortion will not result from the scattering mechanism itself but from the spatial distribution of the scattering, it should be possible to calculate the likely effect by assuming the scattering mechanism is equivalent to the reflection of the signal from a large number of point reflectors distributed within the scattering volume.

As can be seen from Figure 1, if the elevation and azimuth beam shapes of the transmitting and receiving antennas are known, then we could calculate the signal strength and relative phase at the receiver for some nominal transmitter power and a nominal cross section reflector situated at any given point within the scattering volume. It is also possible to calculate the transit time between transmission and reception of this reflected signal.

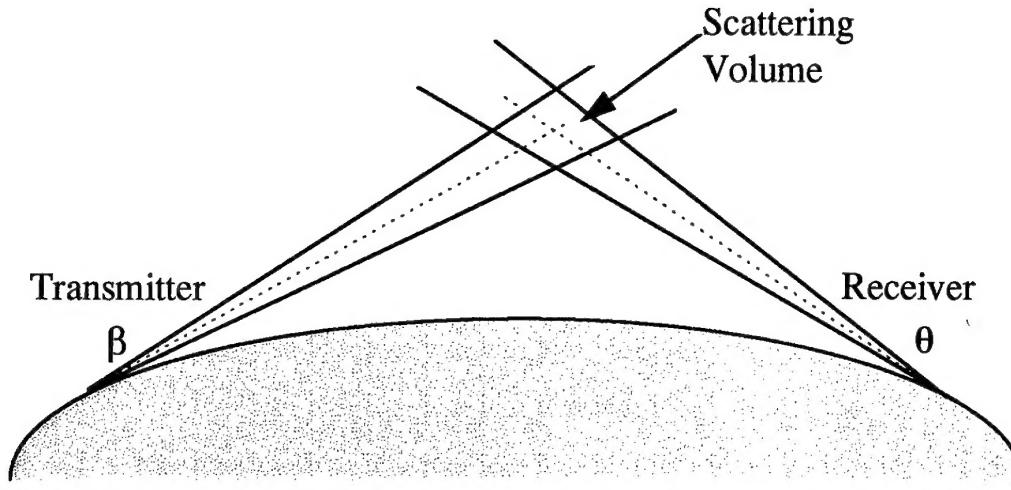


Figure 1: Scattering volume.

It is reasonable to assume that the envelope shape of the signal reflected from a point reflector will be identical to the envelope shape of the transmitted signal. Applying this condition to a large number of identical point reflectors distributed throughout the scattering volume and summing all the individual signals, taking into account the transit time delay of the amplitude envelope and the phase of each signal, then it should be possible to construct the probable amplitude profile of a troposcattered signal for any given transmitted signal envelope shape.

In this project we will not take into account the scattering phenomenon itself, i.e. attenuation, depolarisation and volume scattering effects leading to troposcatter losses. Only a brief theoretical introduction of these effects will be given. Results of computations of troposcatter losses employing known empirical approaches, i.e. NBS, Yeh, Rider etc. were presented in [5].

However, it is believed that the results of the current project which considers the change in the envelope shape due to spatial distribution of the reflectors inside the scattering volume, could be coupled with the results of earlier work [5] in future tasks in order to estimate the combined effect.

## 2. Radio scattering in the troposphere

This section is a brief introduction and overview of the theory of propagation of radio waves via the troposphere.

## 2.1 Interaction processes in the troposphere

There are a number of possible mechanisms whereby radiowaves can interact with the lower atmosphere to produce scattering, these include:

- absorption and dispersion in atmospheric gases (oxygen, water vapour and minor constituents);
- scattering from atmospheric turbulence and scintillation;
- scattering and absorption in populations of hydrometeors (including anisotropic effects, forward scatter, back scatter, and scattering at arbitrary angles);
- scattering and absorption in sand and dust particle populations;
- refraction and reflection in stable atmospheric layers;
- thermal emission from hydrometeors and atmospheric gases.[1]

## 2.2 Theory of scattering and absorption

Attenuation, depolarization and volume scattering of radiowaves due to atmospheric particles are phenomena, which severely limit the performance of telecommunication systems.

Currently, mainly frequencies below 20 GHz are used by communication systems although the use of some millimetre wave frequencies where high absorption occurs has been advocated in the literature for short range secure links.

The basic theory describing different models for attenuation, depolarization and volume scattering is the theory for single-particle scattering. Particle scattering effects become more severe with higher frequencies. This is aggravated by the increasing effect of small particles, such as liquid droplets, which are present in great numbers in the atmosphere.

The problem of single and multiple scattering has been discussed by many authors. Some approaches have different interpretations of formulae and different ways to derive them.

Let us introduce just one model - single scattering approximation, which was described in Reference [3]. Here, the author considered a random medium illuminated by a transmitter. A part of the transmitted wave was scattered by the randomness of the medium and this scattered wave was detected by a receiver (Figure 2).

There was considered a volume  $\delta V$  in the random medium. It was assumed that the randomness of the medium was so slight that the wave incident on  $\delta V$  was almost equal to the incident wave in the absence of the random medium.

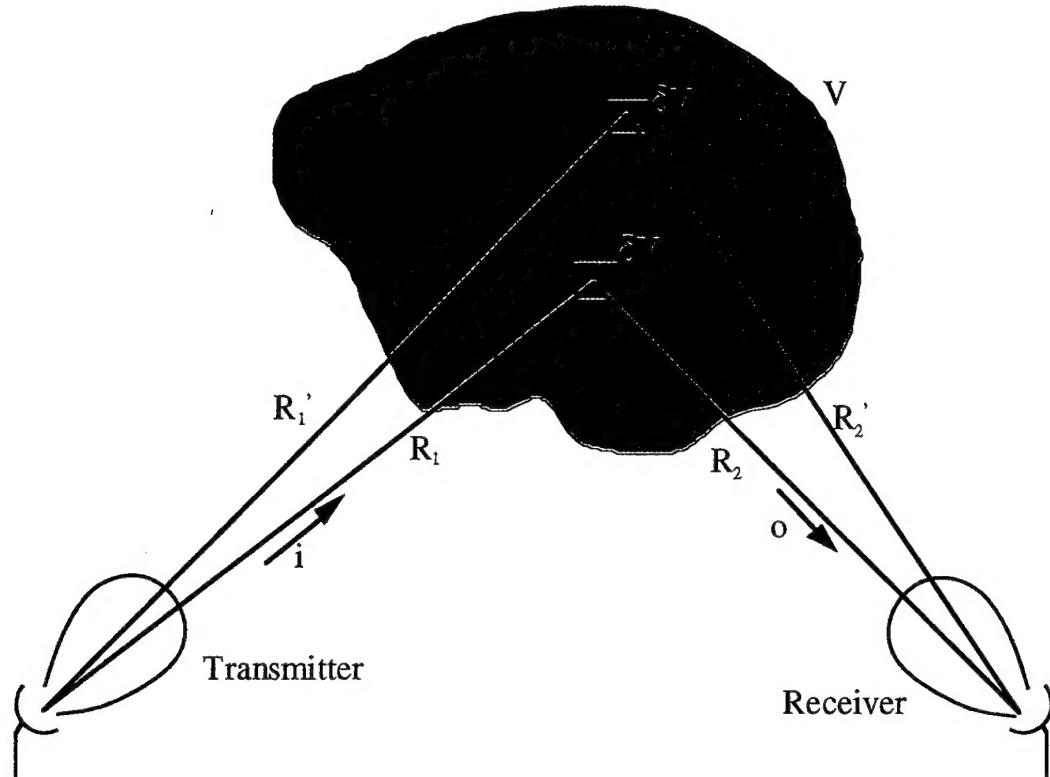


Figure 2: Geometry showing transmitter, receiver and random medium.

It was described by the amount of scattered power due to the random medium in  $\delta V$  in terms of the equivalent scattering cross section per unit volume  $\sigma(0, i)$ , then the received power  $P_r$  is given by the radar equation

$$P_r / P_t = \lambda^2 G_t(i) G_r(0) \sigma(0, i) \delta V / (4\pi)^2 R_1^2 R_2^2 , \quad (1)$$

where  $P_t$  - transmitted power

$G_t, G_r$  - gain functions of the transmitter and receiver antennas in the directions of  $i$  and  $-0$ .

The basic scattering theory must be reviewed in order to find the limitations of its applicability to electromagnetic wave problems.

The theory of single and multiple scattering has been discussed in References [1, 2, 3, 4]. At this time, no references could be found that treat the basic scattering theory, as applied to communication systems, in a completely consistent way. This makes it difficult to understand the scattering theory [1].

### 2.3 Application of the theory of radio scattering in the troposphere to beam communication

Booker and Gordon [4] describe in their work the experiments made in the Caribbean Sea in 1945. The goal of these experiments was to explore the radio consequences of the evaporation-duct that exists at the ocean surface. As a result of this project it was discovered that, at any rate under some circumstances, field strength well beyond the horizon decreases with distance more slowly than could be expected on any existing theory. The wavelength used was 9 cm in this experiment. They found that the unexpectedly high field strengths obtained at long range on 9 cm were not due to duct propagation, and, accounting for the rather violent fading associated with them, it was suggested that a scattering mechanism was involved.

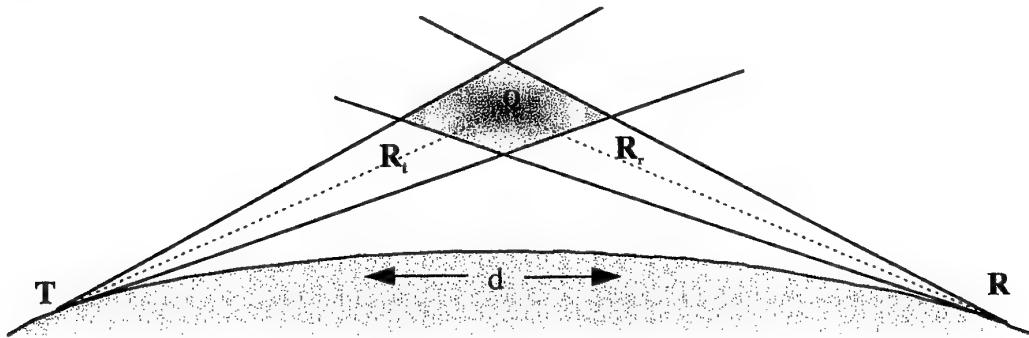


Figure 3: Antennas beams.

Booker and Gordon considered transmission from point T to point R at distance d round the curved surface of the earth by means of beamed antennas pointed more or less at each other as indicated in Figure 3. It was assumed that there were no ducts and that as far as ordinary reflection is concerned propagation was orthodox. It was supposed that both antennas were pointed horizontally at their respective locations, and that their axes lay in the vertical plane through T and R. For simplicity it was considered that the T and R antennas were identical. It was found that if the transmitter and receiver are omnidirectional, scattering is in general important from nearly the whole of the atmosphere above the horizons of both transmitter and receiver. However, in practice, both transmitter and receiver antennas usually have some directivity, and scattering is then important only in the region of atmosphere where the transmitting and receiving beams overlap.

As a result of the Caribbean experiments the following conclusions were made:

1. The modified scale of turbulence is expected to decrease with height above the earth's surface.
2. The theory of atmospheric scattering seems to predict a decrease of scattered field strength with distance that is too low to agree with the observation, in fact the scattering almost certainly decreases with height in most practical cases.
3. The height of the important scattering volume increases with the increase of distance between transmitter and receiver. An associated decrease of the modified scale of atmospheric turbulence would cause the scattering signal received to decrease more rapidly with the increase of range than for a uniformly turbulent atmosphere.
4. The same theory which is used for calculating the scattering signal at long distances may also be used in most cases for calculating the fading range at shorter distances.

### 3. Practical Procedure

First of all, it is necessary to emphasise that, because of the diverse nature of the problem, various approximations should be employed to obtain useful results. Therefore, some useful approximation techniques applicable to a variety of different situations will be presented in this project.

1. We will assume that the transmitter and receiver beam shapes are effectively rectangular.
2. We assign the transmitter to be at the origin ( $x = 1, y = 0$ ) of a two dimensional coordinate system and the receiver to be on the x axis at a point that can be calculated from the great circle distance between the transmitter and receiver sites on the earth surface.
3. We assume both transmitter and receiver beam width to be the same.
4. Then we need to calculate the inclination of the transmitter and receiver antenna beams from the x axis, so that it is possible to calculate the x, y coordinates of the intersecting volume.
5. Next, it is necessary to calculate the coordinates of an array of point reflectors which were initially assumed to be regularly spaced within the intersecting volume although this was later extended to include a uniform density random distribution.

6. For each of the points in the array we then calculate the path length between transmitter and receiver via each point and hence determine the transmit time for each point reflected signal. Because we are interested only in the differences, we subtract the mean transit time from the actual transit time to obtain the delta transit time.
7. Since the signal which is assumed to be reflected from the reflector at each point starts from the transmitter with the same phase, we must now calculate the relative RF phase of each reflected signal by dividing the path length via each point reflector by the free space wavelength of the RF signal and discarding the integer part.
8. Since we have initially chosen to assume a rectangular beam shape and that the path difference from each point reflector will only differ by a small percentage we now assume that all the signals reflected from the point reflectors have the same (unity) amplitude profile.

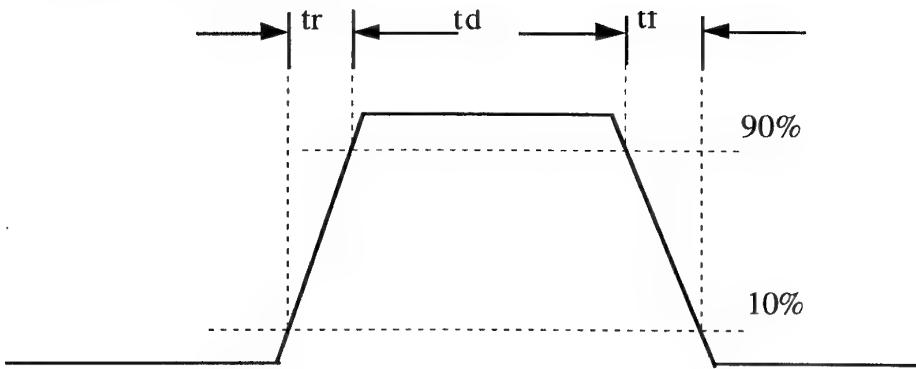


Figure 4: Pulse shape.

9. Now we define a suitable transmitter amplitude profile (pulse shape) by introducing three character-parameters, namely rise time  $t_r$ , fall time  $t_f$ , and duration  $t_d$ .
10. Finally, we produce a temporal plot of the resulting troposcattered waveform shape by doing a vector sum of all the point reflector outputs at each of a large number of time increments encompassing the pulse width and the range of delta transit time. The above is illustrated in Figure 4, and expressed more formally in the following equations:

$$\mathbf{A} = \sum (a_i \cos \varphi_i + j a_i \sin \varphi_i), \quad (2)$$

where  $\Lambda$  - complex amplitude of the resulting envelope signal,

$a_i$  - amplitude of initial envelope signal

$$j = \sqrt{-1}$$

$$\varphi_i = (vl_i/c - \text{Integer}[vl_i/c]) 2\pi$$

$\varphi_i$  - the phase of a signal reflected by point "i" from scattering volume,

$v$  - RF frequency in MHz,

$c$  - the light speed in vacuum in [km/s]'

$l_i$  - the length of the path from the transmitter to receiver via point "i" in [km].

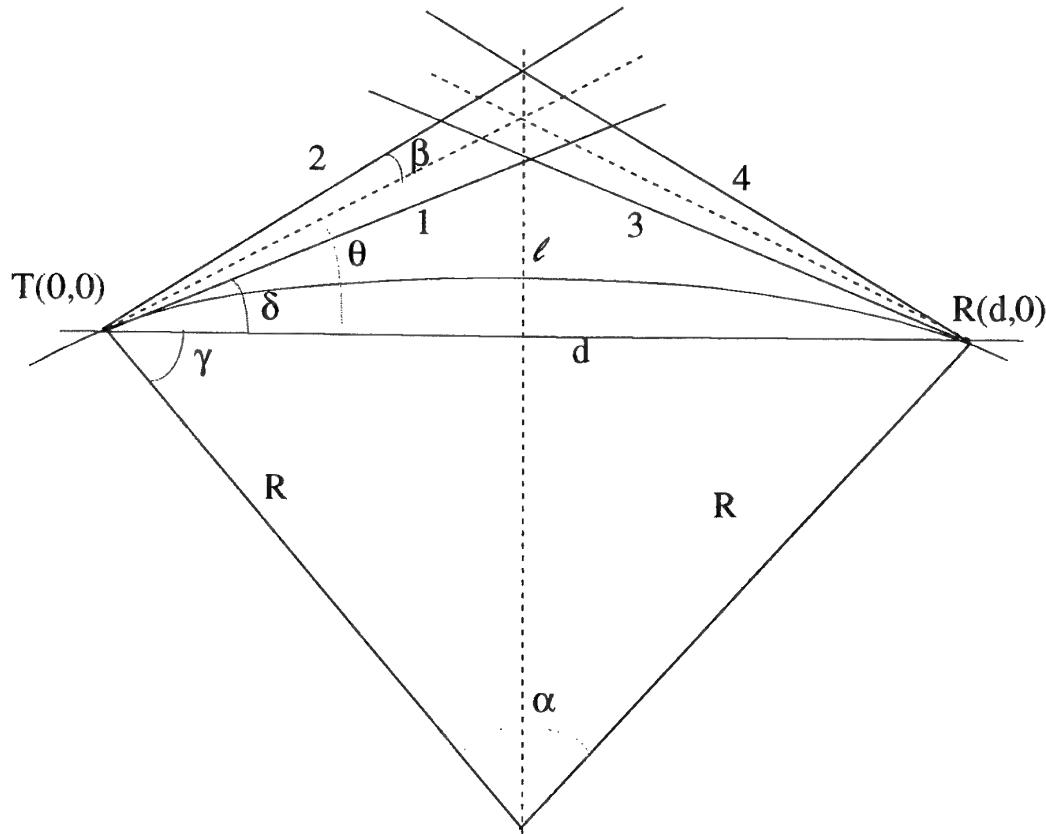


Figure 5: Geometry of beam intersection region.

$$y = \tan(\theta - \beta) x \quad (\text{equation for line 1}) \quad (3)$$

$$y = \tan(\theta + \beta) x \quad (\text{equation for line 2}) \quad (4)$$

Assumption  $\theta_1 = \theta_2 = \theta$

$$\beta_1 = \beta_2 = \beta$$

$$y = -\tan[\theta - \beta] x + b$$

$$0 = -\tan[\theta - \beta] d + b$$

$$d \tan[\theta - \beta] = b$$

$$y = dtan[\theta - \beta] - \tan[\theta - \beta] x, \quad (\text{equation for line 3}) \quad (5)$$

$$y = dtan[\theta + \beta] - \tan[\theta + \beta] x, \quad (\text{equation for line 4}) \quad (6)$$

$$\tan[\theta - \beta] x = dtan[\theta - \beta] - \tan[\theta - \beta] x, \quad (7)$$

$$2\tan[\theta - \beta] x = dtan[\theta - \beta], \quad (8)$$

$$x = d/2, \quad (9)$$

where

R - effective radius of Earth (4/3 physical radius)

$\beta$  - the half beam width angle

l - the distance between the transmitter and the receiver

$\phi$  - the elevation angle of transmitter

n - number of points

$$l = R\alpha$$

$$d^2 = 2R^2 - 2R^2\cos\alpha = 2R(R - R\cos\alpha), \quad (10)$$

$$d = \sqrt{2R(R - R\cos\alpha)}, \quad (11)$$

$$\gamma = (\pi - \alpha)/2, \quad (12)$$

$$\delta = \pi/2 - \gamma = \pi/2 - \pi/2 + \alpha/2 = \alpha/2, \quad (13)$$

$$\theta = \phi + \delta, \quad (14)$$

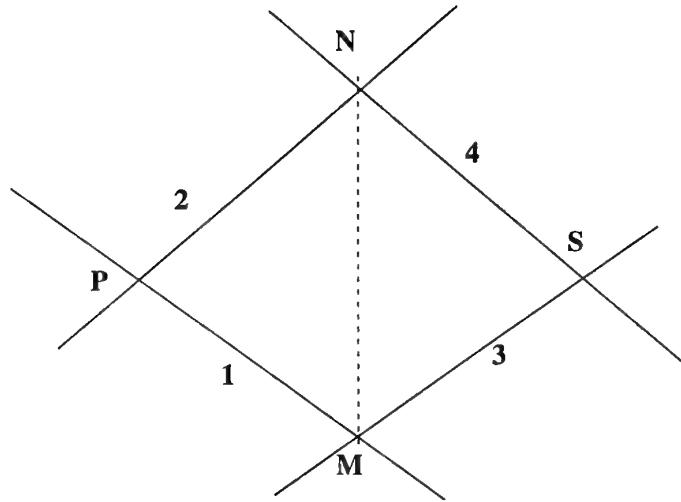


Figure 6: Scattering region.

We have equations for lines 1, 2, 3 and 4.

The ordinate of point N (y coordinate of N) is the maximum y value of the point to be distributed to the area.

The y coordinate of M is the minimum of y coordinate.

In the program the user specifies the numbers of rows,  $r$  and the spacing between the rows is  $\Delta$ .

$$\Delta = \text{distance NM}/r \quad , \quad (15)$$

We know coordinates for the point N. N is specified by  $(x_N, y_N)$ . Take the y coordinate and decrease it's value by  $\Delta$ , i.e.  $y_N - \Delta$ .

From Equation 2 substitute  $y_N - \Delta$  for y and solve for x. This gives us the first point of the first row - point N.

To get the next point, the coordinate will be  $(x_N + \Delta, y_N - \Delta)$ . To find the maximum value of x put  $y_N - \Delta$  into the equation 4 and solve x

While all this is being done, i.e. when each point is determined, we can at this time calculate the distance from transmitter to the receiver via the point. If the coordinates of the point are  $(x_P, y_P)$  then the distance from the transmitter to the receiver is

$$D = \sqrt{((x_P - x_T)^2 + (y_P - y_T)^2)} + \sqrt{((x_P - x_R)^2 + (y_P - y_R)^2)} \quad , \quad (16)$$

where  $x_T, y_T$  - coordinates of the transmitter,

$x_R, y_R$  - coordinates of the receiver,

which are  $(x_T, y_T) = (0, 0)$

$(x_R, y_R) = (d, 0)$

## 4. Operation

The software was developed and runs on an IBM PC and is written in Borland, Turbo C++, version 1.00. The plotting macros require the use of Excel, version 5.0. This section describes how the software can be operated.

### 4.1 Installation

- **pulse\_d.exe, pulse\_e.exe** and **pulse\_r.exe** files should be installed in **c:\tc\bin** directory
- **pulse\_d.xls, pulse\_e.xls** and **pulse\_r.xls** files in any directory

### 4.2 Execution

To obtain a plot of the reflection point distribution:

- run **pulse\_d.exe** in DOS;
- save output to a file called **result\_d.txt**;
- when finished computations, open **pulse\_d.xls** in Excel;
- run the program in “Execute” Sheet of **pulse\_d.xls** workbook.

To obtain a table of data and a plot of the pulse after reflection from a uniform array of points:

- run **pulse\_e.exe** in DOS;
- save output to a file called **result\_e.txt**;
- when finished computations, open **pulse\_e.xls** in Excel;
- run the program in “Execute” Sheet of **pulse\_e.xls** workbook

To obtain a table of data and a plot of the pulse after reflection from a random array of points:

- run pulse\_r.exe in DOS;
- save output to a file named result\_r.txt;
- when finished computations, open pulse\_r.xls in Excel;
- run the program in "Execute" Sheet of pulse\_r.xls workbook.

Note that the programs pulse\_e.xls and pulse\_r.xls are identical except for the result file accessed and the labels on the resulting curves.

## 5. Conclusions

1. Software for computing the modulation envelope after propagation of a given radar signal via the troposphere accounting for the effect of spatial distribution of point reflectors in the scattering volume has been designed and tested.

At this stage, the propagation model is based on point reflectors in a single plane having vertical and horizontal directions with two types of distribution, namely, equidistantly spaced and randomly spaced with uniform density. Elevation angles of both transmitter and receiver were chosen to be equal, as well as their beamwidth angles.

2. The Turbo C++ executable file allows one to plot resulting graphs on the screen and save the data in text format.

A special program was designed in Visual Basic for Excel, which can automatically read the data from the text file generated in Turbo C++ and then plot the graph of envelope amplitude versus time.

*[Note that, with hindsight, it would have been much easier for users if the whole program had been designed in Visual Basic. In this case, a computation could be realised by striking one key either on keyboard or on the mouse.]*

3. Analysis of the results of computations of radar pulse envelope distortion due to tropospheric propagation have shown (Appendix 1, 2):

- pulse shape envelope does change significantly with beamwidth and elevation angle as might be expected since these parameters determine the distance between the shortest and longest paths via the reflection points;
- with uniform distribution there is some evidence of an interference pattern, which is smoothed out to a large degree with a random distribution.

4. The next steps in developing the current model describing radar pulse envelope distortion are envisaged to be:

- extending the analysis to a three dimensional case;
- introducing a vertical variation in the density of the random distribution of reflecting points to reflect the likely variation resulting from the change in density of the troposphere with height;
- introducing some randomness and vertical variation in the amplitude of the reflection from each reflecting point;
- since real radars that we might wish to detect frequently employ a vertical fan shaped ( $\text{cosec}^2$ ) beam, which is unlikely to be the best beam shape to use on the receiver, a new model is needed to take into account different values of beam width for the transmitting and receiving antennas.

## 6. Acknowledgments

This work was done in Electronic Warfare Division under a Technical Support Services contract and the author is grateful for the access to the DSTO library and other facilities that were made available.

The author would like to gratefully acknowledge the contribution from Dr A.Kulessa for the help and advice, he gave me while I was doing this project. Also the author wishes to express her thanks to Mr R. Lindop for help received on the same topic.

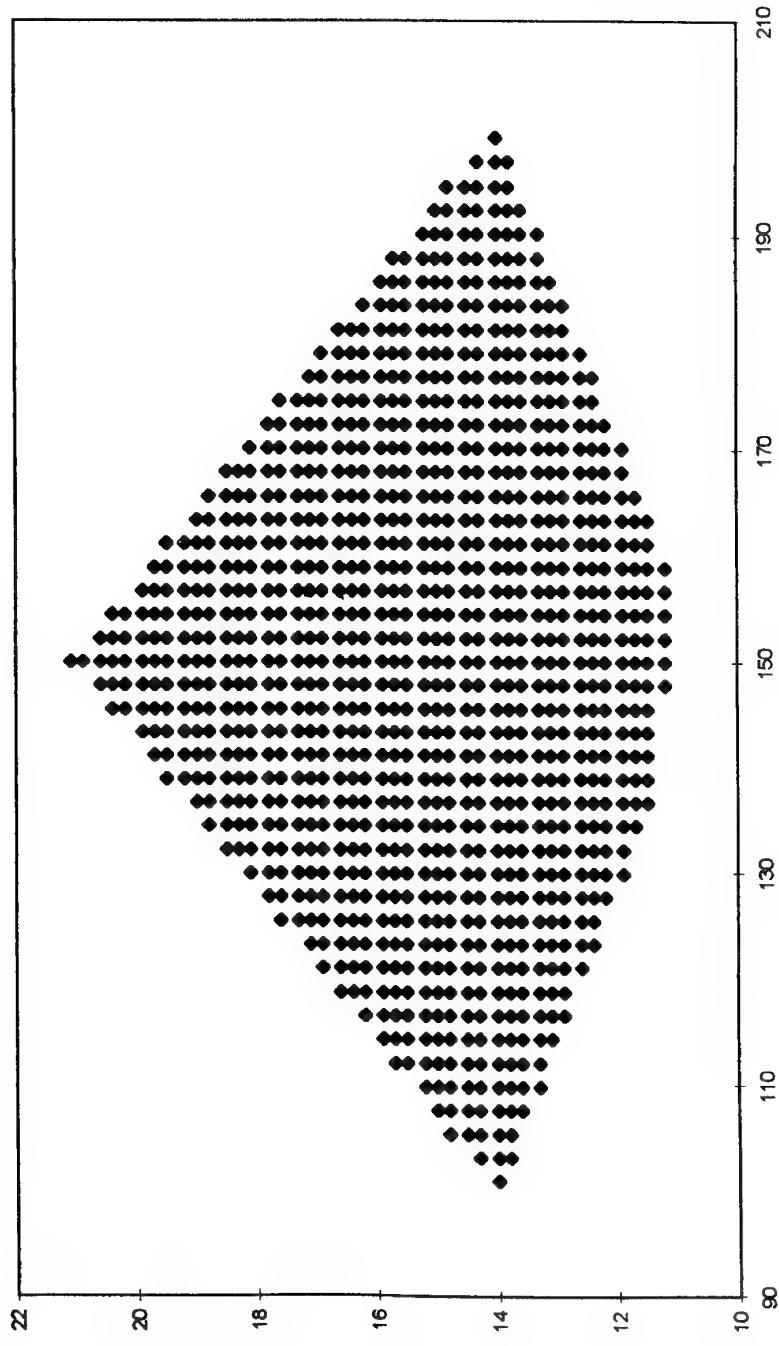
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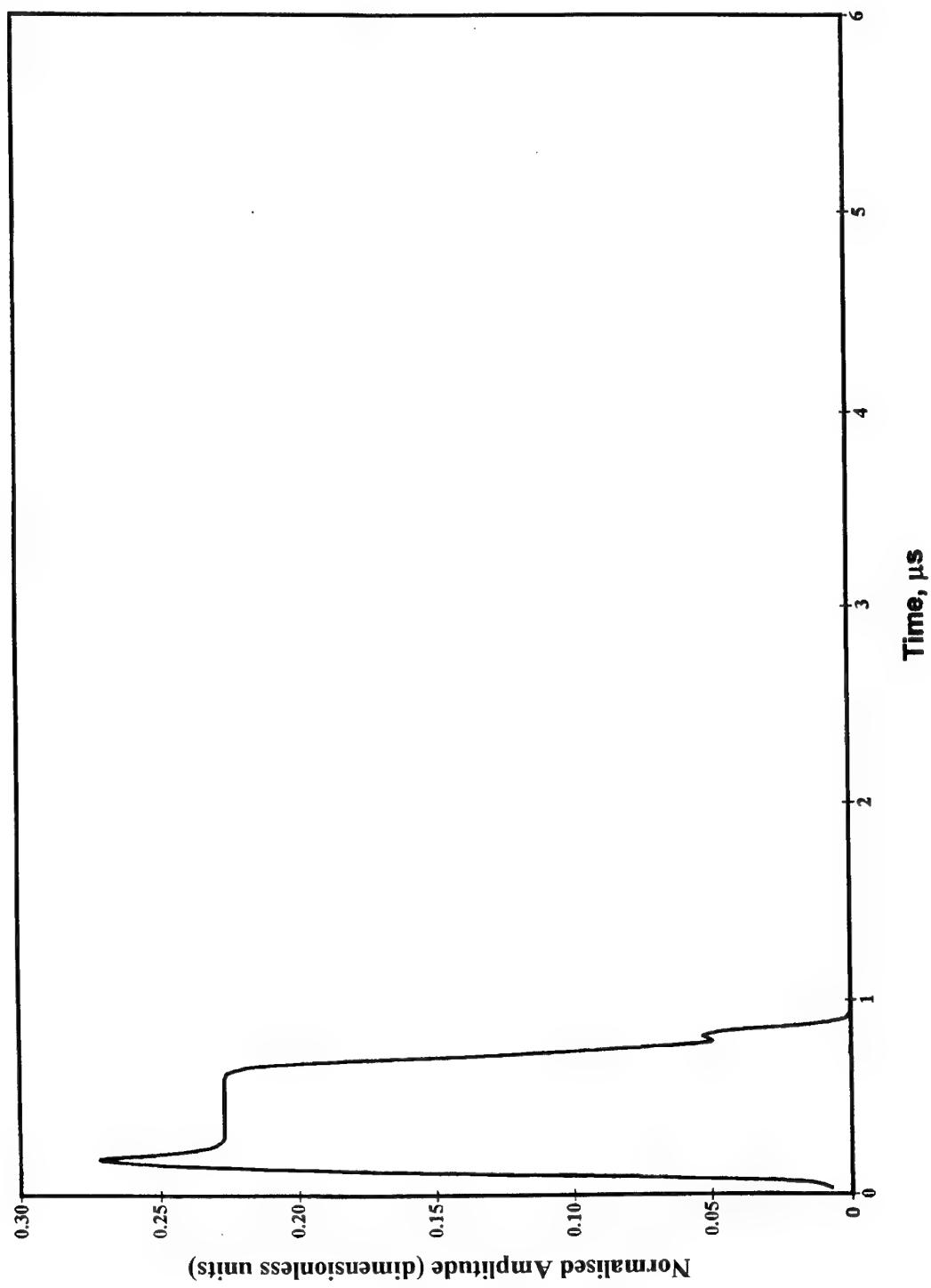
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## Appendix A: Computations of Radar Pulse Envelope Distortion for Uniform Distribution

Grid with uniform distribution of knots



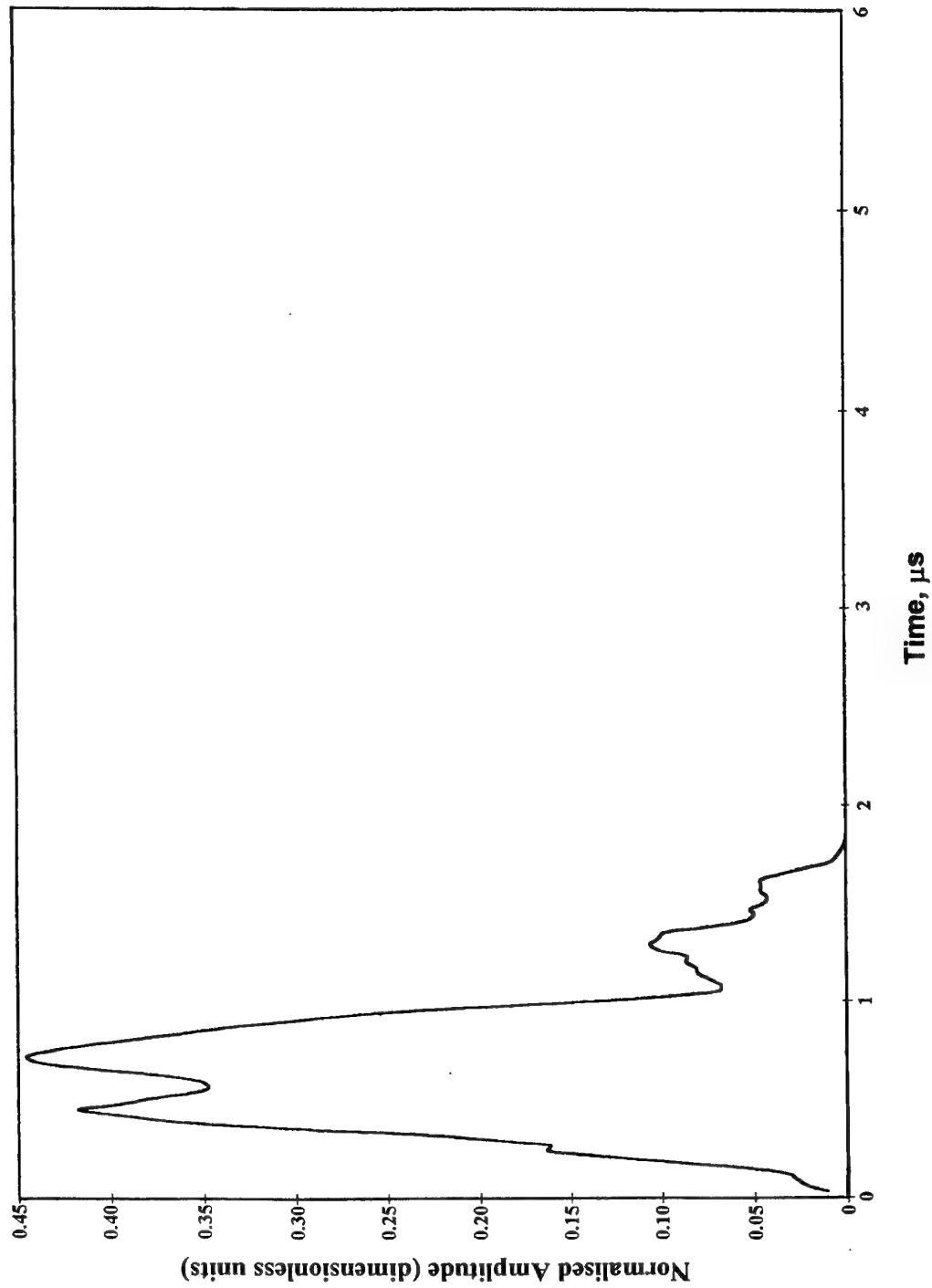
Resulting Envelope Amplitude versus Time (uniform grid)



Beamwidth angle beta (degrees): 1.2  
 Great circle distance l (km): 300  
 Elevation angle phi (degrees): 0.7  
 Number of knots inside the scattering volume n: 1000  
 Operating frequency (MHz): 2830  
 Pulse rise time ( $\mu$ s): 0.1  
 Pulse width ( $\mu$ s): 0.5  
 Pulse fall time ( $\mu$ s): 0.15

i	Time[i]	Amplitude (arbitrary units)		i	Time[i]	Amplitude (arbitrary units)		i	Time[i]	Amplitude (arbitrary units)		i	Time[i]	Amplitude (arbitrary units)	
		Initial	Resulting			Initial	Resulting			Initial	Resulting			Initial	Resulting
1	0.03	0.3	0.733	43	1.29	0	0	85	2.55	0	0	127	3.81	0	0
2	0.06	0.6	1.645	44	1.32	0	0	86	2.58	0	0	128	3.84	0	0
3	0.08	0.8	7.693	45	1.35	0	0	87	2.61	0	0	129	3.87	0	0
4	0.12	1	17.316	46	1.38	0	0	88	2.64	0	0	130	3.9	0	0
5	0.15	1	24.379	47	1.41	0	0	89	2.67	0	0	131	3.93	0	0
6	0.18	1	27.143	48	1.44	0	0	90	2.7	0	0	132	3.96	0	0
7	0.21	1	25.031	49	1.47	0	0	91	2.73	0	0	133	3.99	0	0
8	0.24	1	23.353	50	1.5	0	0	92	2.76	0	0	134	4.02	0	0
9	0.27	1	22.825	51	1.53	0	0	93	2.79	0	0	135	4.05	0	0
10	0.3	1	22.888	52	1.56	0	0	94	2.82	0	0	136	4.08	0	0
11	0.33	1	22.888	53	1.59	0	0	95	2.85	0	0	137	4.11	0	0
12	0.36	1	22.888	54	1.62	0	0	96	2.88	0	0	138	4.14	0	0
13	0.39	1	22.888	55	1.65	0	0	97	2.91	0	0	139	4.17	0	0
14	0.42	1	22.888	56	1.68	0	0	98	2.94	0	0	140	4.2	0	0
15	0.45	1	22.888	57	1.71	0	0	99	2.97	0	0	141	4.23	0	0
16	0.48	1	22.888	58	1.74	0	0	100	3	0	0	142	4.26	0	0
17	0.51	1	22.888	59	1.77	0	0	101	3.03	0	0	143	4.29	0	0
18	0.54	1	22.888	60	1.8	0	0	102	3.06	0	0	144	4.32	0	0
19	0.57	1	22.888	61	1.83	0	0	103	3.09	0	0	145	4.35	0	0
20	0.6	1	22.888	62	1.86	0	0	104	3.12	0	0	146	4.38	0	0
21	0.63	0.6	22.525	63	1.89	0	0	105	3.15	0	0	147	4.41	0	0
22	0.66	0.6	21.595	64	1.92	0	0	106	3.18	0	0	148	4.44	0	0
23	0.69	0.4	17.787	65	1.95	0	0	107	3.21	0	0	149	4.47	0	0
24	0.72	0.2	12.583	66	1.98	0	0	108	3.24	0	0	150	4.5	0	0
25	0.75	0	8.163	67	2.01	0	0	109	3.27	0	0	151	4.53	0	0
26	0.78	0	4.978	68	2.04	0	0	110	3.3	0	0	152	4.56	0	0
27	0.81	0	5.264	69	2.07	0	0	111	3.33	0	0	153	4.59	0	0
28	0.84	0	4.45	70	2.1	0	0	112	3.36	0	0	154	4.62	0	0
29	0.87	0	1.843	71	2.13	0	0	113	3.39	0	0	155	4.65	0	0
30	0.9	0	0.232	72	2.16	0	0	114	3.42	0	0	156	4.68	0	0
31	0.93	0	0.032	73	2.19	0	0	115	3.45	0	0	157	4.71	0	0
32	0.96	0	0	74	2.22	0	0	116	3.48	0	0	158	4.74	0	0
33	0.99	0	0	75	2.25	0	0	117	3.51	0	0	159	4.77	0	0
34	1.02	0	0	76	2.28	0	0	118	3.54	0	0	160	4.8	0	0
35	1.05	0	0	77	2.31	0	0	119	3.57	0	0	161	4.83	0	0
36	1.08	0	0	78	2.34	0	0	120	3.6	0	0	162	4.86	0	0
37	1.11	0	0	79	2.37	0	0	121	3.63	0	0	163	4.89	0	0
38	1.14	0	0	80	2.4	0	0	122	3.66	0	0	164	4.92	0	0
39	1.17	0	0	81	2.43	0	0	123	3.69	0	0	165	4.95	0	0
40	1.2	0	0	82	2.46	0	0	124	3.72	0	0	166	4.98	0	0
41	1.23	0	0	83	2.49	0	0	125	3.75	0	0	167	5.01	0	0
42	1.26	0	0	84	2.52	0	0	126	3.78	0	0	168	5.04	0	0

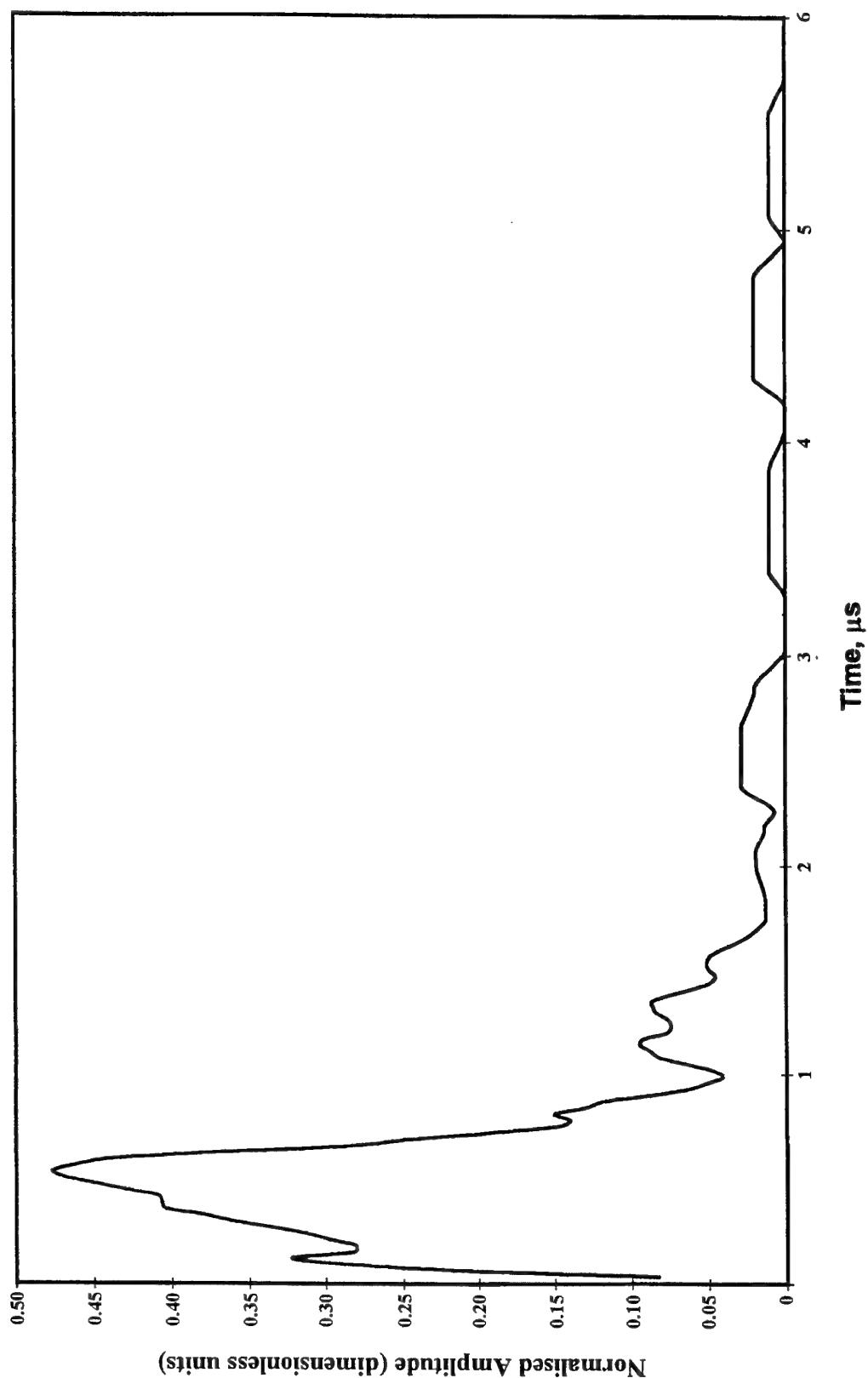
Resulting Envelope Amplitude versus Time (uniform grid)



Beamwidth angle beta (degrees): 2  
 Great circle distance l (km): 300  
 Elevation angle phi (degrees): 5  
 Number of knots inside the scattering volume n: 1000  
 Operating frequency (MHz): 2800  
 Pulse rise time ( $\mu$ s): 0.1  
 Pulse width ( $\mu$ s): 0.5  
 Pulse fall time ( $\mu$ s): 0.15

i	Time[i]		Amplitude (arbitrary units)		i	Time[i]		Amplitude (arbitrary units)		i	Time[i]		Amplitude (arbitrary units)		i	Time[i]		Amplitude (arbitrary units)	
	Initial	Resulting	Initial	Resulting		Initial	Resulting	Initial	Resulting		Initial	Resulting	Initial	Resulting		Initial	Resulting	Initial	Resulting
1	0.03	0.3	1.062	43	1.29	0	10.602	85	2.55	0	0	127	3.81	0	0	169	5.07	0	0
2	0.06	0.6	2.227	44	1.32	0	10.161	86	2.58	0	0	128	3.84	0	0	170	5.1	0	0
3	0.09	0.9	2.725	45	1.35	0	9.798	87	2.61	0	0	129	3.87	0	0	171	5.13	0	0
4	0.12	1	3.268	46	1.38	0	7.356	88	2.64	0	0	130	3.9	0	0	172	5.16	0	0
5	0.15	1	5.524	47	1.41	0	5.425	89	2.67	0	0	131	3.93	0	0	173	5.19	0	0
6	0.18	1	9.197	48	1.44	0	4.941	90	2.7	0	0	132	3.96	0	0	174	5.22	0	0
7	0.21	1	13.169	49	1.47	0	5.154	91	2.73	0	0	133	3.99	0	0	175	5.25	0	0
8	0.24	1	18.307	50	1.5	0	4.411	92	2.76	0	0	134	4.02	0	0	176	5.28	0	0
9	0.27	1	18.142	51	1.53	0	4.223	93	2.79	0	0	135	4.05	0	0	177	5.31	0	0
10	0.3	1	20.073	52	1.56	0	4.565	94	2.82	0	0	136	4.08	0	0	178	5.34	0	0
11	0.33	1	23.888	53	1.59	0	4.54	95	2.85	0	0	137	4.11	0	0	179	5.37	0	0
12	0.36	1	30.251	54	1.62	0	4.576	96	2.88	0	0	138	4.14	0	0	180	5.4	0	0
13	0.39	1	38.069	55	1.65	0	3.43	97	2.91	0	0	139	4.17	0	0	181	5.43	0	0
14	0.42	1	39.101	56	1.68	0	2.202	98	2.94	0	0	140	4.2	0	0	182	5.46	0	0
15	0.45	1	41.745	57	1.71	0	0.875	99	2.97	0	0	141	4.23	0	0	183	5.49	0	0
16	0.48	1	39.632	58	1.74	0	0.511	100	3	0	0	142	4.26	0	0	184	5.52	0	0
17	0.51	1	37.914	59	1.77	0	0.311	101	3.03	0	0	143	4.29	0	0	185	5.55	0	0
18	0.54	1	35.567	60	1.8	0	0.111	102	3.06	0	0	144	4.32	0	0	186	5.58	0	0
19	0.57	1	34.7	61	1.83	0	0	103	3.09	0	0	145	4.35	0	0	187	5.61	0	0
20	0.6	1	35.275	62	1.86	0	0	104	3.12	0	0	146	4.38	0	0	188	5.64	0	0
21	0.63	0.8	37.683	63	1.89	0	0	105	3.15	0	0	147	4.41	0	0	189	5.67	0	0
22	0.66	0.6	41.095	64	1.92	0	0	106	3.18	0	0	148	4.44	0	0	190	5.7	0	0
23	0.69	0.4	43.956	65	1.95	0	0	107	3.21	0	0	149	4.47	0	0	191	5.73	0	0
24	0.72	0.2	44.555	66	1.98	0	0	108	3.24	0	0	150	4.5	0	0	192	5.76	0	0
25	0.75	0	43.177	67	2.01	0	0	109	3.27	0	0	151	4.53	0	0	193	5.79	0	0
26	0.78	0	41.212	68	2.04	0	0	110	3.3	0	0	152	4.56	0	0	194	5.82	0	0
27	0.81	0	38.653	69	2.07	0	0	111	3.33	0	0	153	4.59	0	0	195	5.85	0	0
28	0.84	0	36.077	70	2.1	0	0	112	3.36	0	0	154	4.62	0	0	196	5.88	0	0
29	0.87	0	33.739	71	2.13	0	0	113	3.39	0	0	155	4.65	0	0	197	5.91	0	0
30	0.9	0	30.5	72	2.16	0	0	114	3.42	0	0	156	4.68	0	0	198	5.94	0	0
31	0.93	0	27.018	73	2.19	0	0	115	3.45	0	0	157	4.71	0	0	199	5.97	0	0
32	0.96	0	22.758	74	2.22	0	0	116	3.48	0	0	158	4.74	0	0	200	6	0	0
33	0.99	0	18.266	75	2.25	0	0	117	3.51	0	0	159	4.77	0	0				
34	1.02	0	10.254	76	2.28	0	0	118	3.54	0	0	160	4.8	0	0				
35	1.05	0	6.895	77	2.31	0	0	119	3.57	0	0	161	4.83	0	0				
36	1.08	0	6.736	78	2.34	0	0	120	3.6	0	0	162	4.86	0	0				
37	1.11	0	7.38	79	2.37	0	0	121	3.63	0	0	163	4.89	0	0				
38	1.14	0	7.985	80	2.4	0	0	122	3.66	0	0	164	4.92	0	0				
39	1.17	0	8.08	81	2.43	0	0	123	3.69	0	0	165	4.95	0	0				
40	1.2	0	8.66	82	2.46	0	0	124	3.72	0	0	166	4.98	0	0				
41	1.23	0	8.585	83	2.49	0	0	125	3.75	0	0	167	5.01	0	0				
42	1.26	0	10.117	84	2.52	0	0	126	3.78	0	0	168	5.04	0	0				

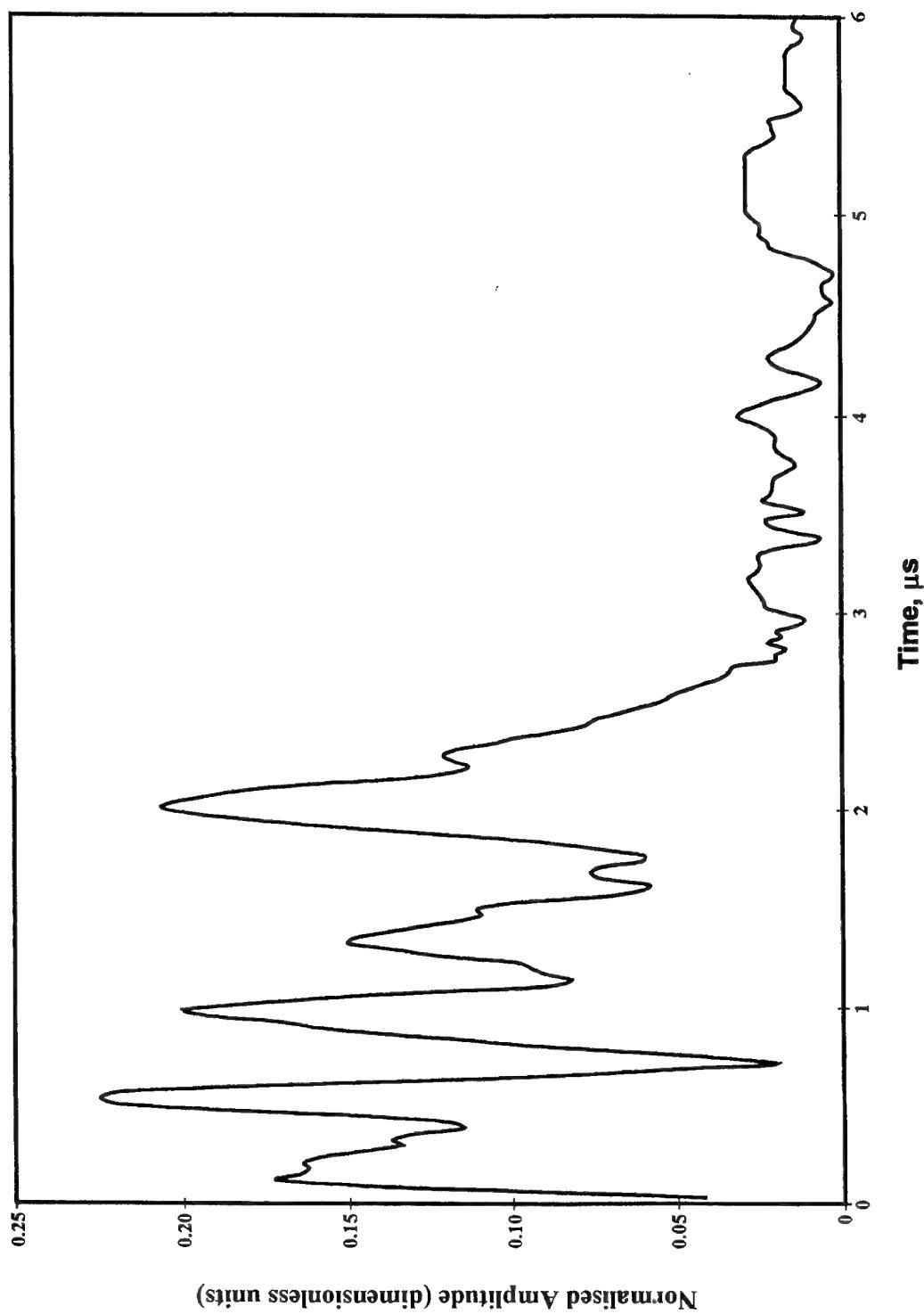
Resulting Envelope Amplitude versus Time (uniform grid)



Beamwidth angle beta (degrees): **4**  
 Great circle distance l (km): **300**  
 Elevation angle phi (degrees): **2.1**  
 Number of knots inside the scattering volume n: **1000**  
 Operating frequency (MHz): **2830**  
 Pulse rise time ( $\mu$ s): **0.1**  
 Pulse width ( $\mu$ s): **0.5**  
 Pulse fall time ( $\mu$ s): **0.15**

i	Time[i]	Amplitude		i	Time[i]	Amplitude		i	Time[i]	Amplitude		i	Time[i]	Amplitude		i	Time[i]	Amplitude									
		(arbitrary units)				(arbitrary units)				(arbitrary units)				(arbitrary units)				(arbitrary units)									
		Initial	Resulting			Initial	Resulting			Initial	Resulting			Initial	Resulting			Initial	Resulting								
1	0.03	0.3	8.325	43	1.29	0	8.341	85	2.55	0	2.813	127	3.81	0	1	169	5.07	0	1								
2	0.06	0.6	20.864	44	1.32	0	8.807	86	2.58	0	2.813	128	3.84	0	1	170	5.1	0	1								
3	0.09	0.9	28.265	45	1.35	0	8.636	87	2.61	0	2.813	129	3.87	0	1	171	5.13	0	1								
4	0.12	1	32.298	46	1.38	0	7.286	88	2.64	0	2.813	130	3.9	0	0.924	172	5.16	0	1								
5	0.15	1	28.21	47	1.41	0	5.836	89	2.67	0	2.785	131	3.93	0	0.724	173	5.19	0	1								
6	0.18	1	28.058	48	1.44	0	4.864	90	2.7	0	2.613	132	3.96	0	0.524	174	5.22	0	1								
7	0.21	1	29.739	49	1.47	0	4.535	91	2.73	0	2.444	133	3.99	0	0.324	175	5.25	0	1								
8	0.24	1	31.349	50	1.5	0	5.002	92	2.76	0	2.282	134	4.02	0	0.124	176	5.28	0	1								
9	0.27	1	33.826	51	1.53	0	5.114	93	2.79	0	2.125	135	4.05	0	0	177	5.31	0	1								
10	0.3	1	36.175	52	1.56	0	4.929	94	2.82	0	2	136	4.08	0	0	178	5.34	0	1								
11	0.33	1	38.007	53	1.59	0	4.348	95	2.85	0	2	137	4.11	0	0	179	5.37	0	1								
12	0.36	1	40.448	54	1.62	0	3.415	96	2.88	0	1.749	138	4.14	0	0	180	5.4	0	1								
13	0.39	1	40.695	55	1.65	0	2.604	97	2.91	0	1.349	139	4.17	0	0	181	5.43	0	1								
14	0.42	1	40.907	56	1.68	0	2.083	98	2.94	0	0.949	140	4.2	0	0.319	182	5.46	0	1								
15	0.45	1	43.108	57	1.71	0	1.641	99	2.97	0	0.549	141	4.23	0	0.919	183	5.49	0	1								
16	0.48	1	44.858	58	1.74	0	1.285	100	3	0	0.149	142	4.26	0	1.519	184	5.52	0	1								
17	0.51	1	46.885	59	1.77	0	1.285	101	3.03	0	0	143	4.29	0	2	185	5.55	0	1								
18	0.54	1	47.881	60	1.8	0	1.285	102	3.06	0	0	144	4.32	0	2	186	5.58	0	0.816								
19	0.57	1	48.215	61	1.83	0	1.285	103	3.09	0	0	145	4.35	0	2	187	5.61	0	0.816								
20	0.6	1	43.815	62	1.86	0	1.381	104	3.12	0	0	146	4.38	0	2	188	5.64	0	0.416								
21	0.63	0.8	37.396	63	1.89	0	1.47	105	3.15	0	0	147	4.41	0	2	189	5.67	0	0.216								
22	0.66	0.6	28.39	64	1.92	0	1.597	106	3.18	0	0	148	4.44	0	2	190	5.7	0	0.016								
23	0.69	0.4	24.574	65	1.95	0	1.731	107	3.21	0	0	149	4.47	0	2	191	5.73	0	0								
24	0.72	0.2	19.463	66	1.98	0	1.864	108	3.24	0	0	150	4.5	0	2	192	5.76	0	0								
25	0.75	0	14.717	67	2.01	0	1.893	109	3.27	0	0	151	4.53	0	2	193	5.79	0	0								
26	0.78	0	13.98	68	2.04	0	1.922	110	3.3	0	0.114	152	4.56	0	2	194	5.82	0	0								
27	0.81	0	14.974	69	2.07	0	1.934	111	3.33	0	0.414	153	4.59	0	2	195	5.85	0	0								
28	0.84	0	12.989	70	2.1	0	1.73	112	3.36	0	0.714	154	4.62	0	2	196	5.88	0	0								
29	0.87	0	11.699	71	2.13	0	1.524	113	3.39	0	1	155	4.65	0	2	197	5.91	0	0								
30	0.9	0	8.735	72	2.16	0	1.354	114	3.42	0	1	156	4.68	0	2	198	5.94	0	0								
31	0.93	0	6.322	73	2.19	0	1.322	115	3.45	0	1	157	4.71	0	2	199	5.97	0	0								
32	0.96	0	5.021	74	2.22	0	0.98	116	3.48	0	1	158	4.74	0	2	200	6	0	0								
33	0.99	0	4.079	75	2.25	0	0.703	117	3.51	0	1	159	4.77	0	2												
34	1.02	0	4.917	76	2.28	0	0.963	118	3.54	0	1	160	4.8	0	1.788												
35	1.05	0	6.483	77	2.31	0	1.68	119	3.57	0	1	161	4.83	0	1.388												
36	1.08	0	8.225	78	2.34	0	2.405	120	3.6	0	1	162	4.86	0	0.988												
37	1.11	0	8.815	79	2.37	0	2.813	121	3.63	0	1	163	4.89	0	0.588												
38	1.14	0	9.458	80	2.4	0	2.813	122	3.66	0	1	164	4.92	0	0.188												
39	1.17	0	9.178	81	2.43	0	2.813	123	3.69	0	1	165	4.95	0	0												
40	1.2	0	7.848	82	2.48	0	2.813	124	3.72	0	1	166	4.98	0	0.278												
41	1.23	0	7.412	83	2.49	0	2.813	125	3.75	0	1	167	5.01	0	0.578												
42	1.28	0	7.625	84	2.52	0	2.813	126	3.78	0	1	168	5.04	0	0.876												

Resulting Envelope Amplitude versus Time (uniform grid)



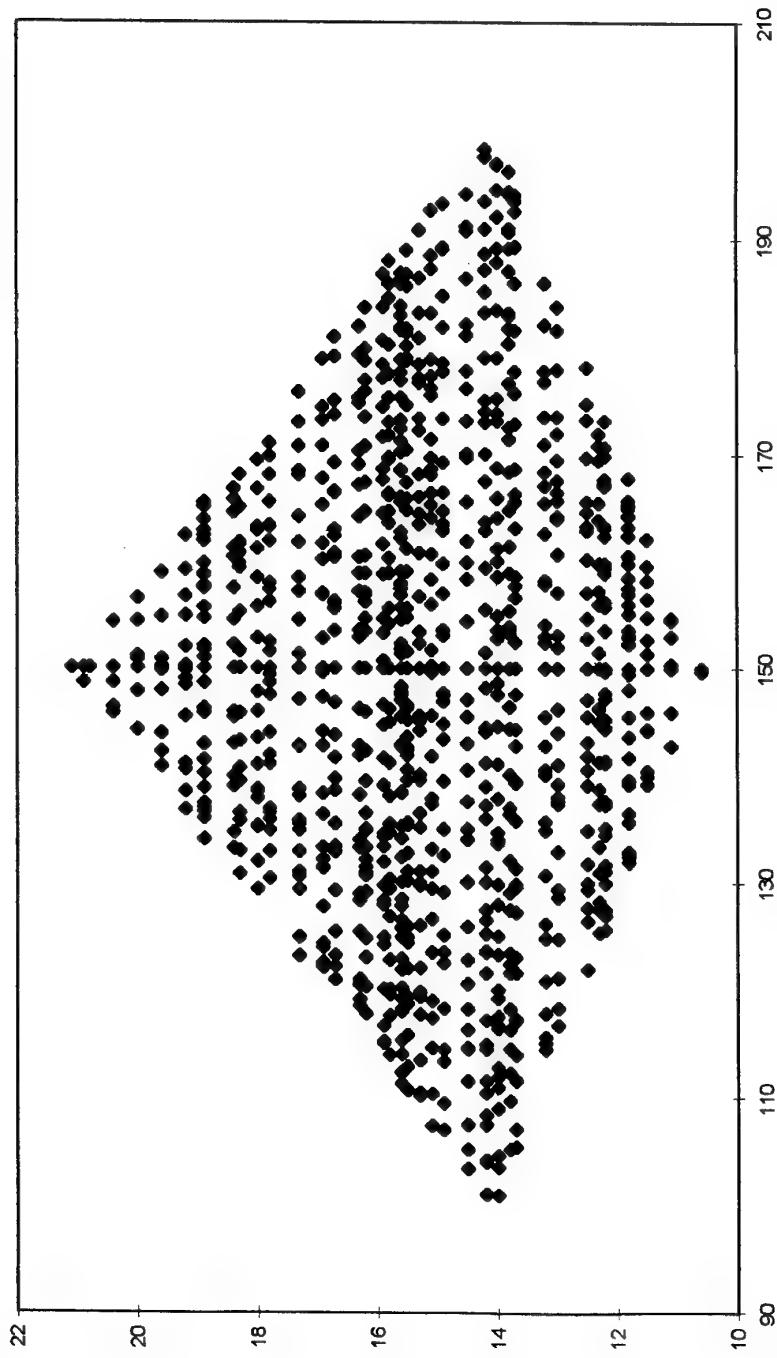
Beamwidth angle beta (degrees): **8**  
 Great circle distance l (km): **300**  
 Elevation angle phi (degrees): **4.1**  
 Number of knots inside the scattering volume n: **1000**  
 Operating frequency (MHz): **2830**  
 Pulse rise time ( $\mu$ s): **0.1**  
 Pulse width ( $\mu$ s): **0.5**  
 Pulse fall time ( $\mu$ s): **0.15**

i	Time[i]	Amplitude (arbitrary units)		i	Time[i]	Amplitude (arbitrary units)		i	Time[i]	Amplitude (arbitrary units)		i	Time[i]	Amplitude (arbitrary units)		i	Time[i]	Amplitude (arbitrary units)	
		Initial	Resulting			Initial	Resulting			Initial	Resulting			Initial	Resulting			Initial	Resulting
1	0.03	0.3	4.2	43	1.29	0	13.484	85	2.55	0	5.451	127	3.81	0	1.793	169	5.07	0	2.838
2	0.06	0.8	9.2	44	1.32	0	15	86	2.58	0	5.115	128	3.84	0	1.981	170	5.1	0	2.836
3	0.09	0.9	14.26	45	1.35	0	14.854	87	2.81	0	4.66	129	3.87	0	1.981	171	5.13	0	2.836
4	0.12	1	17.176	46	1.38	0	13.859	88	2.64	0	4.168	130	3.9	0	1.981	172	5.16	0	2.836
5	0.15	1	15.485	47	1.41	0	12.773	89	2.67	0	3.634	131	3.93	0	2.186	173	5.19	0	2.836
6	0.18	1	16.243	48	1.44	0	11.524	90	2.7	0	3.373	132	3.96	0	2.555	174	5.22	0	2.836
7	0.21	1	16.386	49	1.47	0	10.928	91	2.73	0	3.22	133	3.99	0	3.061	175	5.25	0	2.836
8	0.24	1	15.854	50	1.5	0	11.034	92	2.78	0	2.017	134	4.02	0	2.968	176	5.28	0	2.836
9	0.27	1	14.569	51	1.53	0	9.837	93	2.79	0	1.989	135	4.05	0	2.538	177	5.31	0	2.836
10	0.3	1	13.437	52	1.56	0	7.151	94	2.82	0	1.685	136	4.08	0	2.041	178	5.34	0	2.635
11	0.33	1	13.681	53	1.59	0	8.058	95	2.85	0	2.208	137	4.11	0	1.338	179	5.37	0	2.249
12	0.36	1	13.045	54	1.62	0	5.826	96	2.88	0	1.81	138	4.14	0	0.77	180	5.4	0	1.98
13	0.39	1	11.505	55	1.65	0	7.212	97	2.91	0	1.938	139	4.17	0	0.612	181	5.43	0	2.017
14	0.42	1	11.937	56	1.68	0	7.585	98	2.94	0	1.316	140	4.2	0	1.077	182	5.46	0	2.064
15	0.45	1	14.357	57	1.71	0	7.246	99	2.97	0	1.122	141	4.23	0	1.803	183	5.49	0	2.1
16	0.48	1	18.554	58	1.74	0	6.058	100	3	0	1.761	142	4.26	0	2.102	184	5.52	0	1.45
17	0.51	1	21.987	59	1.77	0	5.97	101	3.03	0	2.285	143	4.29	0	2.176	185	5.55	0	1.144
18	0.54	1	22.489	60	1.8	0	7.327	102	3.06	0	2.339	144	4.32	0	1.903	186	5.58	0	1.233
19	0.57	1	21.963	61	1.83	0	8.785	103	3.09	0	2.446	145	4.35	0	1.476	187	5.61	0	1.424
20	0.6	1	18.688	62	1.86	0	10.634	104	3.12	0	2.603	146	4.38	0	1.22	188	5.64	0	1.838
21	0.63	0.8	13.431	63	1.89	0	13.288	105	3.15	0	2.713	147	4.41	0	1.039	189	5.67	0	1.838
22	0.66	0.8	8.402	64	1.92	0	16.002	106	3.18	0	2.791	148	4.44	0	0.902	190	5.7	0	1.838
23	0.69	0.4	5.118	65	1.95	0	18.004	107	3.21	0	2.539	149	4.47	0	0.788	191	5.73	0	1.636
24	0.72	0.2	2.082	66	1.98	0	19.544	108	3.24	0	2.427	150	4.5	0	0.727	192	5.76	0	1.636
25	0.75	0	3.752	67	2.01	0	10.59	109	3.27	0	2.491	151	4.53	0	0.478	193	5.79	0	1.636
26	0.78	0	6.348	68	2.04	0	20.282	110	3.3	0	2.463	152	4.56	0	0.274	194	5.82	0	1.636
27	0.81	0	9.377	69	2.07	0	18.236	111	3.33	0	1.987	153	4.59	0	0.491	195	5.85	0	1.494
28	0.84	0	11.257	70	2.1	0	18.03	112	3.36	0	0.858	154	4.62	0	0.55	196	5.88	0	1.185
29	0.87	0	13.937	71	2.13	0	18.221	113	3.39	0	0.843	155	4.65	0	0.537	197	5.91	0	1.139
30	0.9	0	15.914	72	2.16	0	13.427	114	3.42	0	1.614	156	4.68	0	0.28	198	5.94	0	1.379
31	0.93	0	17.166	73	2.19	0	11.844	115	3.45	0	2.228	157	4.71	0	0.236	199	5.97	0	1.379
32	0.96	0	19.188	74	2.22	0	11.283	116	3.48	0	2.219	158	4.74	0	0.582	200	6	0	1.289
33	0.99	0	19.947	75	2.25	0	11.751	117	3.51	0	1.153	159	4.77	0	0.935				
34	1.02	0	18.085	76	2.28	0	12.079	118	3.54	0	1.538	160	4.8	0	1.556				
35	1.05	0	15.624	77	2.31	0	11.853	119	3.57	0	2.346	161	4.83	0	2.098				
36	1.08	0	12.471	78	2.34	0	10.515	120	3.6	0	2.158	162	4.86	0	2.189				
37	1.11	0	0.01	79	2.37	0	9.894	121	3.63	0	2.068	163	4.89	0	2.427				
38	1.14	0	8.165	80	2.4	0	8.812	122	3.66	0	2.07	164	4.92	0	2.428				
39	1.17	0	8.997	81	2.43	0	7.762	123	3.69	0	1.996	165	4.95	0	2.438				
40	1.2	0	9.42	82	2.46	0	7.415	124	3.72	0	1.879	166	4.98	0	2.629				
41	1.23	0	9.895	83	2.49	0	8.778	125	3.75	0	1.385	167	5.01	0	2.824				
42	1.26	0	12.134	84	2.52	0	8.125	126	3.78	0	1.481	168	5.04	0	2.838				

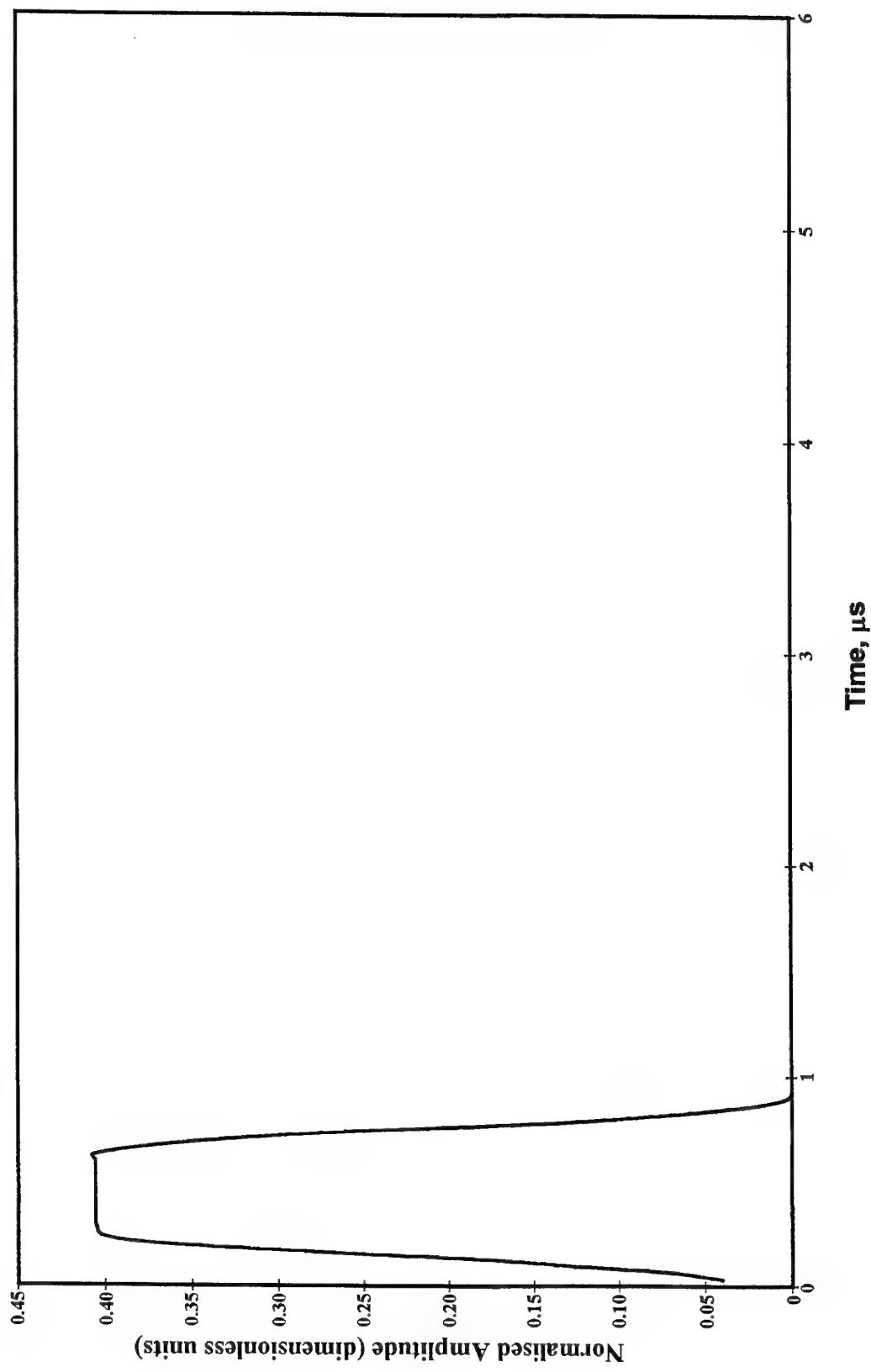
DSTO-TN-0125

## Appendix B: Computations of Radar Pulse Envelope Distortion for Random Distribution

Grid with random distribution of knots

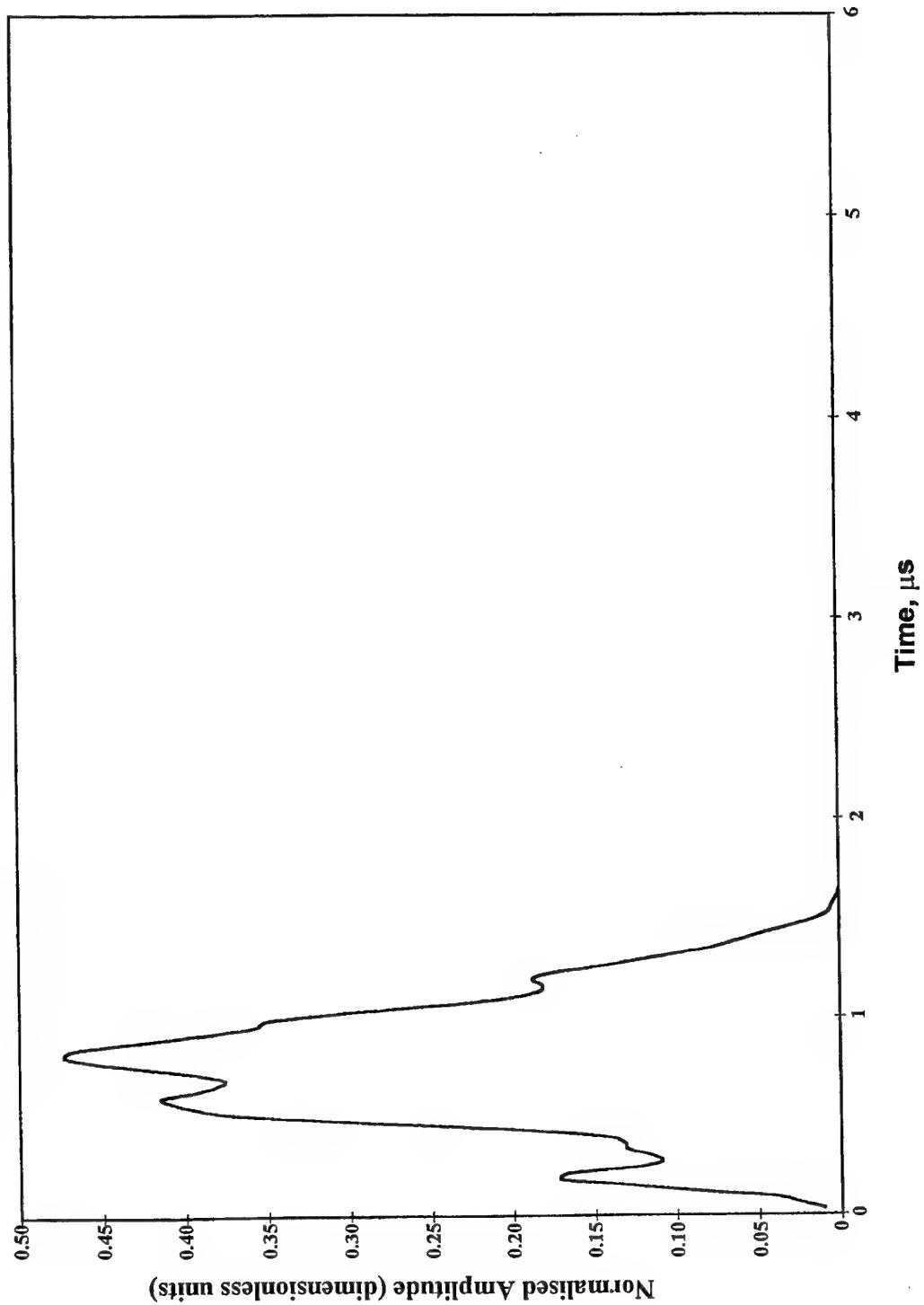


Resulting Envelope Amplitude versus Time (random grid)



Beamwidth angle beta (degrees): 1.2  
 Great circle distance l (km): 300  
 Elevation angle phi (degrees): 0.7  
 Number of knots inside the scattering volume n: 1000  
 Operating frequency (MHz): 2830  
 Pulse rise time ( $\mu$ s): 0.1  
 Pulse width ( $\mu$ s): 0.5  
 Pulse fall time ( $\mu$ s): 0.15

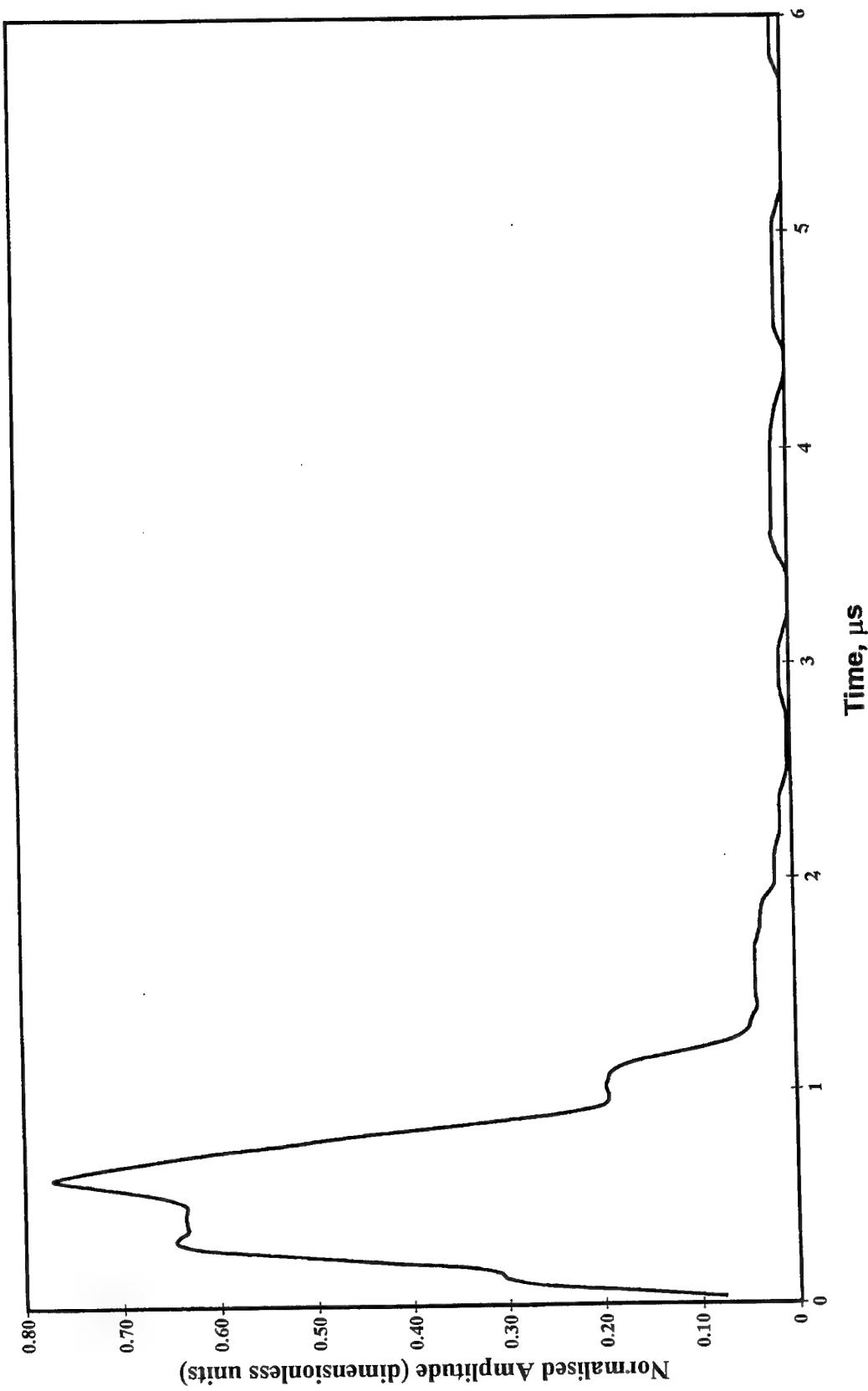
i	Time[i]	Amplitude (arbitrary units)		i	Time[i]	Amplitude (arbitrary units)		i	Time[i]	Amplitude (arbitrary units)		i	Time[i]	Amplitude (arbitrary units)	
		Initial	Resulting			Initial	Resulting			Initial	Resulting			Initial	Resulting
1	0.03	0.3	4.012	43	1.29	0	0	85	2.55	0	0	127	3.81	0	0
2	0.06	0.6	7.129	44	1.32	0	0	88	2.58	0	0	128	3.84	0	0
3	0.09	0.9	12.174	45	1.35	0	0	87	2.81	0	0	129	3.87	0	0
4	0.12	1	17.2	46	1.38	0	0	88	2.84	0	0	130	3.9	0	0
5	0.15	1	25.452	47	1.41	0	0	89	2.67	0	0	131	3.93	0	0
6	0.18	1	33.082	48	1.44	0	0	90	2.7	0	0	132	3.86	0	0
7	0.21	1	38.284	49	1.47	0	0	91	2.73	0	0	133	3.99	0	0
8	0.24	1	40.247	50	1.5	0	0	92	2.76	0	0	134	4.02	0	0
9	0.27	1	40.471	51	1.53	0	0	93	2.79	0	0	135	4.05	0	0
10	0.3	1	40.558	52	1.56	0	0	94	2.82	0	0	136	4.08	0	0
11	0.33	1	40.558	53	1.59	0	0	95	2.85	0	0	137	4.11	0	0
12	0.36	1	40.558	54	1.62	0	0	98	2.88	0	0	138	4.14	0	0
13	0.39	1	40.558	55	1.65	0	0	97	2.91	0	0	139	4.17	0	0
14	0.42	1	40.558	56	1.68	0	0	98	2.94	0	0	140	4.2	0	0
15	0.45	1	40.558	57	1.71	0	0	99	2.97	0	0	141	4.23	0	0
16	0.48	1	40.558	58	1.74	0	0	100	3	0	0	142	4.26	0	0
17	0.51	1	40.558	59	1.77	0	0	101	3.03	0	0	143	4.29	0	0
18	0.54	1	40.558	60	1.8	0	0	102	3.06	0	0	144	4.32	0	0
19	0.57	1	40.558	61	1.83	0	0	103	3.09	0	0	145	4.35	0	0
20	0.6	1	40.558	62	1.88	0	0	104	3.12	0	0	146	4.38	0	0
21	0.63	0.8	40.731	63	1.89	0	0	105	3.15	0	0	147	4.41	0	0
22	0.66	0.6	36.705	64	1.92	0	0	108	3.18	0	0	148	4.44	0	0
23	0.69	0.4	35.273	65	1.95	0	0	107	3.21	0	0	149	4.47	0	0
24	0.72	0.2	30.394	66	1.98	0	0	108	3.24	0	0	150	4.5	0	0
25	0.75	0	22.659	67	2.01	0	0	109	3.27	0	0	151	4.53	0	0
26	0.78	0	14.311	68	2.04	0	0	110	3.3	0	0	152	4.56	0	0
27	0.81	0	8.296	69	2.07	0	0	111	3.33	0	0	153	4.59	0	0
28	0.84	0	4.151	70	2.1	0	0	112	3.36	0	0	154	4.62	0	0
29	0.87	0	1.484	71	2.13	0	0	113	3.39	0	0	155	4.65	0	0
30	0.9	0	0.2	72	2.16	0	0	114	3.42	0	0	156	4.68	0	0
31	0.93	0	0	73	2.19	0	0	115	3.45	0	0	157	4.71	0	0
32	0.96	0	0	74	2.22	0	0	116	3.48	0	0	158	4.74	0	0
33	0.99	0	0	75	2.25	0	0	117	3.51	0	0	159	4.77	0	0
34	1.02	0	0	76	2.28	0	0	118	3.54	0	0	160	4.8	0	0
35	1.05	0	0	77	2.31	0	0	119	3.57	0	0	161	4.83	0	0
36	1.08	0	0	78	2.34	0	0	120	3.6	0	0	162	4.86	0	0
37	1.11	0	0	79	2.37	0	0	121	3.63	0	0	163	4.89	0	0
38	1.14	0	0	80	2.4	0	0	122	3.66	0	0	164	4.92	0	0
39	1.17	0	0	81	2.43	0	0	123	3.69	0	0	165	4.95	0	0
40	1.2	0	0	82	2.46	0	0	124	3.72	0	0	166	4.98	0	0
41	1.23	0	0	83	2.49	0	0	125	3.75	0	0	167	5.01	0	0
42	1.26	0	0	84	2.52	0	0	128	3.78	0	0	168	5.04	0	0



Beamwidth angle beta (degrees): **2**  
 Great circle distance l (km): **300**  
 Elevation angle phi (degrees): **4**  
 Number of knots inside the scattering volume n: **1000**  
 Operating frequency (MHz): **2800**  
 Pulse rise time ( $\mu$ s): **0.1**  
 Pulse width ( $\mu$ s): **0.5**  
 Pulse fall time ( $\mu$ s): **0.15**

i	Time[i]	Amplitude		i	Time[i]	Amplitude		i	Time[i]	Amplitude		i	Time[i]	Amplitude		i	Time[i]	Amplitude	
		Initial	Resulting			Initial	Resulting			Initial	Resulting			Initial	Resulting			Initial	Resulting
1	0.03	0.3	1.055	43	1.29	0	12.828	85	2.55	0	0	127	3.81	0	0	169	5.07	0	0
2	0.06	0.6	2.412	44	1.32	0	10.248	88	2.58	0	0	128	3.84	0	0	170	5.1	0	0
3	0.09	0.9	4.094	45	1.35	0	7.891	87	2.61	0	0	129	3.87	0	0	171	5.13	0	0
4	0.12	1	6.946	46	1.38	0	6.667	88	2.64	0	0	130	3.9	0	0	172	5.16	0	0
5	0.15	1	13.161	47	1.41	0	5.317	89	2.67	0	0	131	3.93	0	0	173	5.19	0	0
6	0.18	1	17.091	48	1.44	0	3.978	90	2.7	0	0	132	3.96	0	0	174	5.22	0	0
7	0.21	1	16.751	49	1.47	0	2.868	91	2.73	0	0	133	3.99	0	0	175	5.25	0	0
8	0.24	1	12.496	50	1.5	0	1.374	92	2.76	0	0	134	4.02	0	0	176	5.28	0	0
9	0.27	1	10.864	51	1.53	0	0.693	93	2.79	0	0	135	4.05	0	0	177	5.31	0	0
10	0.3	1	11.494	52	1.56	0	0.493	94	2.82	0	0	136	4.08	0	0	178	5.34	0	0
11	0.33	1	13.042	53	1.59	0	0.293	95	2.85	0	0	137	4.11	0	0	179	5.37	0	0
12	0.36	1	13.158	54	1.82	0	0.093	96	2.88	0	0	138	4.14	0	0	180	5.4	0	0
13	0.39	1	13.967	55	1.85	0	0	97	2.91	0	0	139	4.17	0	0	181	5.43	0	0
14	0.42	1	17.627	56	1.88	0	0	98	2.94	0	0	140	4.2	0	0	182	5.46	0	0
15	0.45	1	24.203	57	1.71	0	0	99	2.97	0	0	141	4.23	0	0	183	5.49	0	0
16	0.48	1	30.908	58	1.74	0	0	100	3	0	0	142	4.26	0	0	184	5.52	0	0
17	0.51	1	36.937	59	1.77	0	0	101	3.03	0	0	143	4.29	0	0	185	5.55	0	0
18	0.54	1	39.337	60	1.8	0	0	102	3.06	0	0	144	4.32	0	0	186	5.58	0	0
19	0.57	1	40.892	61	1.83	0	0	103	3.09	0	0	145	4.35	0	0	187	5.61	0	0
20	0.6	1	41.491	62	1.86	0	0	104	3.12	0	0	146	4.38	0	0	188	5.64	0	0
21	0.63	0.8	39.367	63	1.89	0	0	105	3.15	0	0	147	4.41	0	0	189	5.67	0	0
22	0.66	0.6	38.169	64	1.92	0	0	106	3.18	0	0	148	4.44	0	0	190	5.7	0	0
23	0.69	0.4	37.601	65	1.95	0	0	107	3.21	0	0	149	4.47	0	0	191	5.73	0	0
24	0.72	0.2	39.528	66	1.98	0	0	108	3.24	0	0	150	4.5	0	0	192	5.76	0	0
25	0.75	0	42.72	67	2.01	0	0	109	3.27	0	0	151	4.53	0	0	193	5.79	0	0
26	0.78	0	45.483	68	2.04	0	0	110	3.3	0	0	152	4.56	0	0	194	5.82	0	0
27	0.81	0	47.33	69	2.07	0	0	111	3.33	0	0	153	4.59	0	0	195	5.85	0	0
28	0.84	0	46.909	70	2.1	0	0	112	3.36	0	0	154	4.62	0	0	196	5.88	0	0
29	0.87	0	44.501	71	2.13	0	0	113	3.39	0	0	155	4.65	0	0	197	5.91	0	0
30	0.9	0	41.048	72	2.16	0	0	114	3.42	0	0	156	4.68	0	0	198	5.94	0	0
31	0.93	0	37.939	73	2.19	0	0	115	3.45	0	0	157	4.71	0	0	199	5.97	0	0
32	0.96	0	35.688	74	2.22	0	0	116	3.48	0	0	158	4.74	0	0	200	6	0	0
33	0.99	0	35.073	75	2.25	0	0	117	3.51	0	0	159	4.77	0	0				
34	1.02	0	31.582	76	2.28	0	0	118	3.54	0	0	160	4.8	0	0				
35	1.05	0	28.922	77	2.31	0	0	119	3.57	0	0	161	4.83	0	0				
36	1.08	0	22.673	78	2.34	0	0	120	3.6	0	0	162	4.86	0	0				
37	1.11	0	19.573	79	2.37	0	0	121	3.63	0	0	163	4.89	0	0				
38	1.14	0	18.178	80	2.4	0	0	122	3.66	0	0	164	4.92	0	0				
39	1.17	0	18.173	81	2.43	0	0	123	3.69	0	0	165	4.95	0	0				
40	1.2	0	18.727	82	2.46	0	0	124	3.72	0	0	166	4.98	0	0				
41	1.23	0	17.545	83	2.49	0	0	125	3.75	0	0	167	5.01	0	0				
42	1.26	0	15.012	84	2.52	0	0	126	3.78	0	0	168	5.04	0	0				

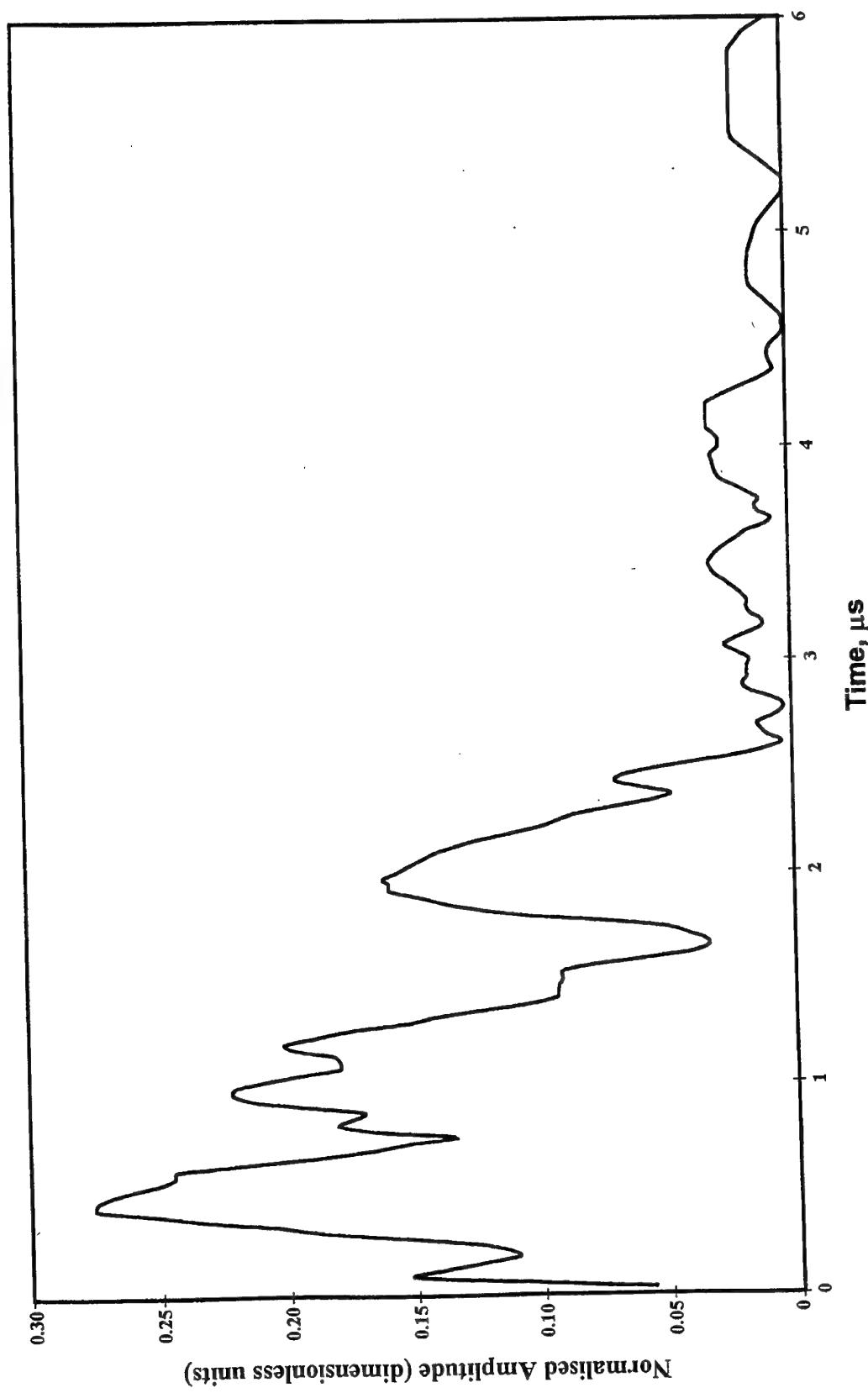
Resulting Envelope Amplitude versus Time (random grid)



Beamwidth angle beta (degrees): **4**  
 Great circle distance l (km): **300**  
 Elevation angle phi (degrees): **2.1**  
 Number of knots inside the scattering volume n: **1000**  
 Operating frequency (MHz): **2830**  
 Pulse rise time ( $\mu$ s): **0.1**  
 Pulse width ( $\mu$ s): **0.5**  
 Pulse fall time ( $\mu$ s): **0.15**

i	Time[i]	Amplitude (arbitrary units)		i	Time[i]	Amplitude (arbitrary units)		i	Time[i]	Amplitude (arbitrary units)		i	Time[i]	Amplitude (arbitrary units)	
		Initial	Resulting			Initial	Resulting			Initial	Resulting			Initial	Resulting
1	0.03	0.3	7.796	43	1.29	0	4.73	85	2.55	0	0.349	127	3.81	0	1.573
2	0.06	0.6	16.812	44	1.32	0	4.598	86	2.58	0	0.347	128	3.84	0	1.573
3	0.09	0.9	26.132	45	1.35	0	4.287	87	2.81	0	0.347	129	3.87	0	1.573
4	0.12	1	30.115	46	1.38	0	3.913	88	2.64	0	0.347	130	3.9	0	1.573
5	0.15	1	31.009	47	1.41	0	3.91	89	2.67	0	0.347	131	3.93	0	1.573
6	0.18	1	35.371	48	1.44	0	3.998	90	2.7	0	0.347	132	3.96	0	1.573
7	0.21	1	44.845	49	1.47	0	3.998	91	2.73	0	0.343	133	3.99	0	1.573
8	0.24	1	53.907	50	1.5	0	3.998	92	2.76	0	0.414	134	4.02	0	1.547
9	0.27	1	61.915	51	1.53	0	3.998	93	2.79	0	0.552	135	4.05	0	1.477
10	0.3	1	64.519	52	1.56	0	3.998	94	2.82	0	0.72	136	4.08	0	1.432
11	0.33	1	64.268	53	1.59	0	3.998	95	2.85	0	0.901	137	4.11	0	1.337
12	0.36	1	63.382	54	1.62	0	3.998	96	2.88	0	1	138	4.14	0	1.21
13	0.39	1	63.526	55	1.65	0	3.998	97	2.91	0	1	139	4.17	0	1.144
14	0.42	1	63.575	56	1.68	0	3.998	98	2.94	0	1	140	4.2	0	0.954
15	0.45	1	63.529	57	1.71	0	3.628	99	2.97	0	1	141	4.23	0	0.701
16	0.48	1	63.522	58	1.74	0	3.618	100	3	0	1	142	4.26	0	0.487
17	0.51	1	65.248	59	1.77	0	3.449	101	3.03	0	1	143	4.29	0	0.287
18	0.54	1	85.462	60	1.8	0	3.491	102	3.06	0	1	144	4.32	0	0.087
19	0.57	1	73.087	61	1.83	0	3.374	103	3.09	0	0.891	145	4.35	0	0
20	0.6	1	77.048	62	1.86	0	3.279	104	3.12	0	0.891	146	4.38	0	0
21	0.63	0.8	75.013	63	1.89	0	3.062	105	3.15	0	0.491	147	4.41	0	0
22	0.66	0.6	70.84	64	1.92	0	2.574	106	3.18	0	0.291	148	4.44	0	0
23	0.69	0.4	66.171	65	1.95	0	2.047	107	3.21	0	0.091	149	4.47	0	0.253
24	0.72	0.2	61.137	66	1.98	0	1.855	108	3.24	0	0	150	4.5	0	0.553
25	0.75	0	54.312	67	2.01	0	1.855	109	3.27	0	0	151	4.53	0	0.853
26	0.78	0	49.432	68	2.04	0	1.855	110	3.3	0	0	152	4.56	0	1
27	0.81	0	43.191	69	2.07	0	1.855	111	3.33	0	0	153	4.59	0	1
28	0.84	0	35.877	70	2.1	0	1.855	112	3.36	0	0	154	4.62	0	1
29	0.87	0	28.604	71	2.13	0	1.748	113	3.39	0	0	155	4.65	0	1
30	0.9	0	23.317	72	2.16	0	1.54	114	3.42	0	0.094	156	4.68	0	1
31	0.93	0	19.953	73	2.19	0	1.368	115	3.45	0	0.394	157	4.71	0	1
32	0.96	0	19.325	74	2.22	0	1.254	116	3.48	0	0.694	158	4.74	0	1
33	0.99	0	19.441	75	2.25	0	1.254	117	3.51	0	1.07	159	4.77	0	1
34	1.02	0	19.608	76	2.28	0	1.254	118	3.54	0	1.281	160	4.8	0	1
35	1.05	0	19.424	77	2.31	0	1.254	119	3.57	0	1.517	161	4.83	0	1
36	1.08	0	19.193	78	2.34	0	1.254	120	3.6	0	1.674	162	4.86	0	1
37	1.11	0	18.16	79	2.37	0	1.254	121	3.63	0	1.589	163	4.89	0	1
38	1.14	0	16.131	80	2.4	0	1.089	122	3.66	0	1.558	164	4.92	0	1
39	1.17	0	13.096	81	2.43	0	0.813	123	3.69	0	1.573	165	4.95	0	1
40	1.2	0	8.805	82	2.46	0	0.599	124	3.72	0	1.573	166	4.98	0	1
41	1.23	0	6.981	83	2.49	0	0.422	125	3.75	0	1.573	167	5.01	0	1
42	1.26	0.	5.491	84	2.52	0	0.325	126	3.78	0	1.573	168	5.04	0	1

Resulting Envelope Amplitude versus Time (random grid)



Beamwidth angle beta (degrees): **8**  
 Great circle distance l (km): **300**  
 Elevation angle phi (degrees): **4.1**  
 Number of knots inside the scattering volume n: **1000**  
 Operating frequency (MHz): **2830**  
 Pulse rise time ( $\mu$ s): **0.1**  
 Pulse width ( $\mu$ s): **0.5**  
 Pulse fall time ( $\mu$ s): **0.15**

i	Time[i]	Amplitude		i	Time[i]	Amplitude		i	Time[i]	Amplitude		i	Time[i]	Amplitude		i	Time[i]	Amplitude									
		(arbitrary units)				(arbitrary units)				(arbitrary units)				(arbitrary units)				(arbitrary units)									
		Initial	Resulting			Initial	Resulting			Initial	Resulting			Initial	Resulting			Initial	Resulting								
1	0.03	0.3	5.753	43	1.29	0	15.318	85	2.55	0	2.051	127	3.81	0	1.984	169	5.07	0	0.746								
2	0.08	0.8	11.228	44	1.32	0	14.151	86	2.58	0	1.001	128	3.84	0	2.516	170	5.1	0	0.546								
3	0.09	0.9	15.123	45	1.35	0	12.421	87	2.61	0	0.398	129	3.87	0	2.722	171	5.13	0	0.346								
4	0.12	1	13.946	46	1.38	0	10.485	88	2.64	0	0.923	130	3.9	0	2.815	172	5.16	0	0.146								
5	0.15	1	12.391	47	1.41	0	9.325	89	2.67	0	1.181	131	3.93	0	2.884	173	5.19	0	0								
6	0.18	1	11.029	48	1.44	0	8.272	90	2.7	0	1.302	132	3.96	0	2.921	174	5.22	0	0								
7	0.21	1	11.398	49	1.47	0	9.231	91	2.73	0	0.736	133	3.99	0	2.634	175	5.25	0	0.017								
8	0.24	1	12.885	50	1.5	0	9.074	92	2.76	0	0.347	134	4.02	0	2.597	176	5.28	0	0.317								
9	0.27	1	15.375	51	1.53	0	8.073	93	2.79	0	0.381	135	4.05	0	2.746	177	5.31	0	0.617								
10	0.3	1	18.887	52	1.56	0	7.829	94	2.82	0	0.837	136	4.08	0	3.031	178	5.34	0	0.921								
11	0.33	1	20.709	53	1.59	0	5.798	95	2.85	0	1.59	137	4.11	0	3.059	179	5.37	0	1.289								
12	0.36	1	23.251	54	1.62	0	3.9	96	2.88	0	1.855	138	4.14	0	3.059	180	5.4	0	1.58								
13	0.39	1	25.258	55	1.65	0	3.314	97	2.91	0	1.87	139	4.17	0	3.059	181	5.43	0	1.873								
14	0.42	1	27.503	56	1.68	0	3.512	98	2.94	0	1.677	140	4.2	0	3.02	182	5.46	0	1.968								
15	0.45	1	27.478	57	1.71	0	4.181	99	2.97	0	1.85	141	4.23	0	2.529	183	5.49	0	1.968								
16	0.48	1	27.035	58	1.74	0	5.134	100	3	0	1.598	142	4.26	0	1.988	184	5.52	0	1.968								
17	0.51	1	26.151	59	1.77	0	7.474	101	3.03	0	2.072	143	4.29	0	1.402	185	5.55	0	1.968								
18	0.54	1	25.054	60	1.8	0	10.685	102	3.06	0	2.509	144	4.32	0	0.874	186	5.58	0	1.968								
19	0.57	1	24.458	61	1.83	0	12.503	103	3.09	0	2.19	145	4.35	0	0.487	187	5.61	0	1.968								
20	0.6	1	24.397	62	1.86	0	13.74	104	3.12	0	1.57	146	4.38	0	0.581	188	5.64	0	1.968								
21	0.63	0.8	21.88	63	1.89	0	14.767	105	3.15	0	1.06	147	4.41	0	0.668	189	5.67	0	1.968								
22	0.66	0.8	18.845	64	1.92	0	15.938	106	3.18	0	1.11	148	4.44	0	0.874	190	5.7	0	1.968								
23	0.69	0.4	16.793	65	1.95	0	15.858	107	3.21	0	1.507	149	4.47	0	0.522	191	5.73	0	1.968								
24	0.72	0.2	15.34	66	1.98	0	16.076	108	3.24	0	1.657	150	4.5	0	0.258	192	5.76	0	1.968								
25	0.75	0	13.446	67	2.01	0	15.494	109	3.27	0	1.624	151	4.53	0	0.088	193	5.79	0	1.968								
26	0.76	0	16.36	68	2.04	0	15.031	110	3.3	0	1.818	152	4.56	0	0.101	194	5.82	0	1.968								
27	0.81	0	17.969	69	2.07	0	14.504	111	3.33	0	2.124	153	4.59	0	0.101	195	5.85	0	1.968								
28	0.84	0	17.486	70	2.1	0	14.007	112	3.36	0	2.416	154	4.62	0	0.275	196	5.88	0	1.78								
29	0.87	0	17.026	71	2.13	0	13.225	113	3.39	0	2.789	155	4.65	0	0.538	197	5.91	0	1.584								
30	0.9	0	19.215	72	2.16	0	12.344	114	3.42	0	2.988	156	4.68	0	0.802	198	5.94	0	1.388								
31	0.93	0	21.397	73	2.19	0	11.065	115	3.45	0	3.09	157	4.71	0	1.068	199	5.97	0	0.976								
32	0.96	0	22.121	74	2.22	0	9.923	116	3.48	0	2.934	158	4.74	0	1.33	200	6	0	0.597								
33	0.99	0	22.063	75	2.25	0	9.135	117	3.51	0	2.892	159	4.77	0	1.385												
34	1.02	0	20.891	76	2.28	0	8.407	118	3.54	0	2.339	160	4.8	0	1.385												
35	1.05	0	19.594	77	2.31	0	6.917	119	3.57	0	1.931	161	4.83	0	1.385												
36	1.08	0	17.93	78	2.34	0	5.483	120	3.6	0	1.589	162	4.86	0	1.385												
37	1.11	0	17.908	79	2.37	0	4.724	121	3.63	0	0.95	163	4.89	0	1.389												
38	1.14	0	18.162	80	2.4	0	5.805	122	3.66	0	0.88	164	4.92	0	1.293												
39	1.17	0	19.675	81	2.43	0	6.888	123	3.69	0	1.124	165	4.95	0	1.218												
40	1.2	0	20.098	82	2.46	0	6.6	124	3.72	0	1.25	166	4.98	0	1.144												
41	1.23	0	18.87	83	2.48	0	5.273	125	3.75	0	1.114	167	5.01	0	1.07												
42	1.26	0	17.475	84	2.52	0	3.803	126	3.78	0	1.5	168	5.04	0	0.946												



## Prediction of Radar Pulse Envelope Distortion due to Tropospheric Propagation

Marina Oszerova

(DSTO-TN-0125)

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